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Why Magnetic Measurements?



"Magnetism is an experimental science" Mike Coey, 2010

"No clear understanding of magnetism can be attained without a sound knowledge of the way in which magnetic properties are measured." B.D. Cullity & CD Graham: Introduction to Magnetic Materials, 2009

What needs to be measured ?



M(H) loop and domains

Reversal of Ni₈₁Fe₁₉ (30 nm) / NiO (30 nm)



M(H) loop and domains

Reversal of $Ni_{81}Fe_{19}$ (30 nm) / NiO (30 nm)



M(H) loop and domains

Reversal of Ni₈₁Fe₁₉ (30 nm) / NiO (30 nm)



What needs to be measured ?

Magnetization curve

Domain scale masurements (Magnetic Imaging)

Saturation magnetization M_s

Crystal- or other anisotropy constants K

Exchange or stiffness constant A

Magnetostriction constants λ

Magnetoresistance

Damping constants α Resonance frequency f_{res}



Magnetic order (neutrons)

and more...

Contents of lecture

- 1. Production of magnetic field
- 2. Measurement of magnetic field strength
- 3. Measurements to determine magnetic material parameters & properties
 - 3.1. Magnetic measurements
 - 3.2. Mechanical measurements
 - 3.3. Resonance techniques
 - 3.4. Dilatometric measurements
 - 3.5. Domain methods
- 4. Domain scale measurements (Magnetic Imaging)

UNITS FOR MAGNETIC PROPERTIES

Quantity	Symbol	Gaussian & cgs emu ^a	Conversion factor, C ^b	SI & rationalized mks ^c
Magnetic flux density, magnetic induction	В	gauss (G) ^d	10 ⁻⁴	tesla (T), Wb/m ²
Magnetic flux	Φ	maxwell (Mx), G·cm ²	10 ⁻⁸	weber (Wb), volt second (V $\!\cdot\!s)$
Magnetic potential difference, magnetomotive force	<i>U</i> , <i>F</i>	gilbert (Gb)	10/4π	ampere (A)
Magnetic field strength, magnetizing force	Η	oersted (Oe), ^e Gb/cm	$10^{3}/4\pi$	A/m ^f
(Volume) magnetization ^g	М	emu/cm ^{3 h}	10 ³	A/m
(Volume) magnetization	$4\pi M$	G	$10^{3}/4\pi$	A/m
Magnetic polarization, intensity of magnetization	J, I	emu/cm ³	$4\pi \times 10^{-4}$	T, Wb/m ^{2 i}
(Mass) magnetization	σ, Μ	emu/g	$1 4\pi \times 10^{-7}$	A·m²/kg Wb·m/kg
Magnetic moment	m	emu, erg/G	10 ⁻³	$A \cdot m^2$, joule per tesla (J/T)
Magnetic dipole moment	j	emu, erg/G	$4\pi \times 10^{-10}$	Wb·m ⁱ
(Volume) susceptibility	χ, к	dimensionless, emu/cm ³	4π $(4\pi)^2 \times 10^{-7}$	dimensionless henry per meter (H/m), Wb/(A·m)
(Mass) susceptibility	χ _ρ , κ _ρ	cm ³ /g, emu/g	$4\pi \times 10^{-3}$ $(4\pi)^2 \times 10^{-10}$	m ³ /kg H·m ² /kg
(Molar) susceptibility	χ_{mol}, κ_{mol}	cm ³ /mol, emu/mol	$4\pi \times 10^{-6}$ $(4\pi)^2 \times 10^{-13}$	m ³ /mol H·m ² /mol
Permeability	μ	dimensionless	$4\pi \times 10^{-7}$	H/m, Wb/(A·m)
Relative permeability ^j	μ_r	not defined		dimensionless
(Volume) energy density, energy product ^k	W	erg/cm ³	10 ⁻¹	J/m ³
Demagnetization factor	D , N	dimensionless	$1/4\pi$	dimensionless

a. Gaussian units and cgs emu are the same for magnetic properties. The defining relation is $B = H + 4\pi M$.

b. Multiply a number in Gaussian units by C to convert it to SI (e.g., $1 \text{ G} \times 10^{-4} \text{ T/G} = 10^{-4} \text{ T}$).

c. SI (Système International d'Unités) has been adopted by the National Bureau of Standards. Where two conversion factors are given, the upper one is recognized under, or consistent with, SI and is based on the definition $B = \mu_0(H+M)$, where $\mu_0 = 4\pi \times 10^{-7}$ H/m. The lower one is not recognized under SI and is based on the definition $B = \mu_0(H+J)$, where the symbol I is often used in place of J.

d. 1 gauss = 10^5 gamma (γ).

e. Both oersted and gauss are expressed as $cm^{-1/2} \cdot g^{1/2} \cdot s^{-1}$ in terms of base units.

- f. A/m was often expressed as "ampere-turn per meter" when used for magnetic field strength.
- g. Magnetic moment per unit volume.
- h. The designation "emu" is not a unit.
- *i.* Recognized under SI, even though based on the definition $B = \mu_0 H + J$. See footnote c.
- j. $\mu_r = \mu/\mu_0 = 1 + \chi$, all in SI. μ_r is equal to Gaussian μ .
- k. B·H and $\mu_0 M \cdot H$ have SI units J/m³; M·H and B·H/4 π have Gaussian units erg/cm³.

R. B. Goldfarb and F. R. Fickett, U.S. Department of Commerce, National Bureau of Standards, Boulder, Colorado 80303, March 1985 NBS Special Publication 696 For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, DC 20402

Magnetic Units

In this presentation: SI units

$$B = \mu_0(H + M) = \mu_0H + J$$

$$B, J: [T] = \left[\frac{V \sec}{m^2}\right]$$
$$H, M: \left[\frac{A}{m}\right]$$

* Although SI unit of field is A/m, it is common to express field strength in units of $\mu_0 H = B$ [Tesla]

from IEEE Magn. Soc. webpage

http://www.ieeemagnetics.org/images/ stories/magnetic_units.pdf

For reading

B.D. Cullity and C.D. Graham: Introduction to Magnetic Materials. IEEE Press and Wiley (2009)

S. Tumanski: Handbook of Magnetic Measurements. CRC Press Taylor & Francis (2009)

F. Fiorillo: Measurement and Characterization of Magnetic Materials. Elsevier Academic Press (2004)

R. Hilzinger and W. Rodewald: Magnetic Materials. Edited by Vacuumschmelze GmbH, Publicis Publishing, Erlangen (2013)

D.C. Jiles: Introduction to Magnetism and Magnetic Materials. Chapman & Hall, London (1995)

G. Bertotti: Hysteresis in Magnetism. Academic Press, New York (1998)

M. Coey: Magnetism and Magnetic Materials. Cambridge University Press (2010)

A. Hubert and R.S.: Magnetic Domains. Springer Verlag (1998)

Many figures in this presentation are taken from these references special thanks to the authors

Two possibilities to generate magnetic field:



By electrical currents flowing in conductor → electromagnetic coils



By exploiting the ordered array of quantummechanical electronic currents circulating in a magnetic material (→ permanent magnets)











1.1 Electromagnetic coils



Solenoid with one layer of winding:

$$H(x) = \frac{n \cdot I}{l} \cdot \left\{ \frac{(l+2x)}{2\sqrt{[d^2 + (l+2x)^2]}} + \frac{(l-2x)}{2\sqrt{[d^2 + (l-2x)^2]}} \right\}$$

Field at centre:

$$H(x=0) = \frac{n \cdot I}{l} \cdot \frac{l}{\sqrt{[d^2+l^2]}}$$

Long solenoid $(l \gg d)$: $H(x=0) = \frac{n \cdot I}{l}$

1.1 Electromagnetic coils

Remarks:

 Higher field: better increase n/l by adding more layers of winding rather than increasing current

 $H \sim I$, but *heat* ~ $I^2 R$

Thus doubling number of winding layers and keeping current constant will double H, R, and amount of *heat*; whereas doubling of current will double H, but will quadruple *heat*

 Typical field: 0.1 T , higher field requires cooling

Solenoid

Solenoid with one layer of winding:

$$H(x) = \frac{n \cdot I}{l} \cdot \left\{ \frac{(l+2x)}{2\sqrt{[d^2 + (l+2x)^2]}} + \frac{(l-2x)}{2\sqrt{[d^2 + (l-2x)^2]}} \right\}$$

Field at centre:

$$H(x=0) = \frac{n \cdot I}{l} \cdot \frac{l}{\sqrt{[d^2 + l^2]}}$$

Long solenoid
$$(l \gg d)$$
:
 $H(x=0) = \frac{n \cdot I}{l}$

1.1 Electromagnetic coils High-Field Solenoid: Bitter magnet

- High field: requires large power input → two major design problems:
- 1) Large amount of heat (note: maintaining magnetic field by current is process of zero efficiency: all input power goes into heat)
- 2) Mechanical strength to resist large forces acting on current carriers has to be provided

Bitter magnet:

- Winding composed of Cu disks, ~30 cm diameter
- Insulated from each other, clamped together
- Rotated by 20°: overlap = conduction path
- Cooling water pumped through holes,
- Helical current path, acts like solenoid
- Typical field: 45 Tesla in 30 mm bore, requires current of 67.000 A, power input of 20 MW
- Requires large motor-generator sets



1.1 Electromagnetic coils High-field Solenoid: Pulsed Fields

High pulsed fields by discharging capacitor bank through conventional solenoid



In shown arrangement with given inductance L of solenoid, an oscillating damped discharge is obtined (switch S₂ open). If S₂ is closed at maximum field, the diode prevents capacitor from discharging with reversed polarity and current decays from maximum value with time constant $\tau_1 = L/R$

1.1 Electromagnetic coils Superconducting Solenoids

- DC fields up to about 20 T can be obtained by superconducting solenoids, commonly used for fields above 2 T
- Type II superconductor with high critical current and critical field: Nb-Ti or Nb₃Sn
- Cooling of coil by liquid helium (4.2 K), sample temperature up to room temperature
- Shortcut of superconducting coil: persistant mode, no power consumption over months
- Danger: quench by local heating



1.2 Electromagnets

DC fields up to 2 T, most commonly used magnetic field source in labs

Evolution of the electromagnet:



Solenoid, flux density at center C:

$$B = \mu_0 H = \mu_0 \frac{n \cdot I}{l}$$

Solenoid with iron rod, flux density at center C:

$$B = \mu_0(H + M) = \mu_0 \mu_r H = \mu_r \mu_0 \frac{n \cdot I}{l}$$

Iron has multiplied field due to the current by factor of μ_r :

same field occurs just outside rod at P \rightarrow large field obtained with low current (e.g. $H_{coil} = 1 \text{ mT}$, $\mu_r = 2000$: $H_{outside} = 2 \text{ T}$) Problem: flux lines outside iron diverge and field decreases rapidly

Bended iron rod with gap:

Flux travels directly from pole to pole across gap. Contribution of iron to gap field (if saturated) = 2.15 T

1.2 Electromagnets

DC fields up to 2 T, most commonly used magnetic field source in labs

Evolution of the electromagnet:



Electromagnet:

- Windings close to gap
- Core and yoke made of iron, annealed for high permeability
- Windings water-cooled
- Pole diameter: up to 30 cm
- Flat poles for uniform field
- Tapered poles: free poles formed on tappered surfaces contribute to field at gap center, can achieve fields higher than $\mu_0 M_s$ (> 3T for gap length of 5-10 mm). Optimum taper angle: 54,74°
- Pole pieces made of CoFe (M_s about 10% higher than for pure Fe)

1.2 Electromagnets

DC fields up to 2 T, most commonly used magnetic field source in la

Finite element simulations: lines and contour maps of induction ${\cal B}$



1.3 Permanent Magnets

Fields up to ~2T by appropriate arrangement of permanent magnets



Technical design of Halbach cylinder: array of uniformly magnetized NdFeB magnets, uniform field accross diameter



Two concentric Halbach arrays: vectorial addition of flux density in centre. By synchronous but opposite rotation, the field strength can be continuously varied



One-sided field by superposition



Simplification of above aray: continuously varying field by counter rotation of 4 transversly magnetized rods

2. Measurement of Magnetic Field Strength



- Hall probe = plate made of InSb or GaAs semiconductor
- $H\mbox{-field}$ perpendicular to plate distorts current path and emf $U_{\rm H}$ is developed between a and b
- Multirange instruments, sensitive to field range from μT to 3T
- Uncertainty in field reading: 1-5% in hand-held Gaussmeters
- Alternating fields up to some 10 kHz can be measured
- Calibration by accuratly known fields required
- Low-field probes: zero must be set with probe in magnetically shielded cylinder to eliminate Earth's field





- Instrument to integrate voltage from pick-up coil is called fluxmeter

 electronic integrator (based on capacitive feedback around operational amplifier)
 that provides voltage output
- With $B = \varphi/A$ (flux density in pick-up coil of cross section A):

$$\int U(t) dt = -n A \Delta B \text{ [Vsec]}$$

Fluxmeter measures changes in flux density



- Instrument to integrate voltage from pick-up coil is called fluxmeter

 electronic integrator (based on capacitive feedback around operational amplifier)
 that provides voltage output
 Measurement of the provides voltage output
- With $B = \varphi/A$ (flux density in pick-up coil of cross section A):

$$\int U(t) dt = -n A \Delta B \text{ [Vsec]}$$

Fluxmeter measures changes in flux density Measurement of constant field: search coil must be moved to zero-field region, or rotated through 180°

2.3 Fluxgate Magnetometer





- Current through the drive: one half core generates B along $H_{\rm ext}$, other half core in opposite direction
- $H_{\text{ext}} = 0$: two half cores go into and come out of saturation at same time $\rightarrow B$ -fields cancel \rightarrow no net change of flux in sense winding \rightarrow no voltage induced
- $H_{\text{ext}} \neq 0$: one half core comes out of saturation sooner, other half core later \rightarrow net flux change \rightarrow voltage \rightarrow two spikes in voltage for each transition in drive
- Size and phase of induced spikes \rightarrow magnitude and direction of $H_{\rm ext}$
- Typical field range: 0.1 nT 1 mT (used in e.g. geomagnetic and archeological surveys)



2.4 Magnetic Potentiometer (Rogowski-Chattok coil)

- Tightly wound coil whose ends lie in same plane, attached to magnetic sample
- Field at surface of magnetic sample is the same as internal field
- If no current flows in coil: line integral $\oint Hdl$ around dotted path must be zero:

$$\int_{A}^{B} H \, dl + \int_{B}^{A} H \, dL = 0$$

• If field is uniform along L:

$$\int_{B}^{A} H \, dL = H \, \Delta L = -\int_{A}^{B} H \, dl$$

- Output of coil is connected to integrator
- Move Chattok coil to region of zero field: output of integrator proportional to (constant) H between A and B; $H = H_i$
- Is used to measure magnetic field in fluxclosing yokes (like singe sheet testers for electrical steel)



2.5 Proton Precession Magnetometer

- High-precision measurement of weak magnetic field (like Earth's field, with uncertainty 1 ppm), also used for calibration
- Relies on Nuclear Magnetic Resonance (NMR): applyig magnetic field → magnetic moment of nucleus rotates in selected quantum directions with resonance frequency which strictly depends on value of field
- Principle:
 - (1) sample (e.g. 1 liter of water, kerosine...) is exposed to strong dc magnetic field B_0 (~ 10 mT) perpendicluar to the measured field B_x . B_0 aligns certain fraction of proton moments along coil direction
 - (2) B_0 switched-off \rightarrow magnetic moments of protons align along B_x by decaying precession movement. Frequency of precession is

measured by measuring frequency of induced voltage in coil. Frequency depends precisely on B_x .

 Typical precessional frequency: a few kilohertz



2.5 Proton Precession Magnetometer



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 \Rightarrow magnetic moments of protons align along $B_{\rm X}$ by decaying



2.6 SQUID Magnetometer

- SQUID: Superconducting Quantum Interference Device magnetometer
- Based on tunneling of superconducting electrons across narrow insulating gap, called Josephson junction
- Ring-shaped device, superconducting current from A to B, equal currents pass through each junction
- Changing magnetic flux through ring: induces "screening" current in ring (Faraday's law) which generates magnetic field that cancels external flux. Induced current adds to measuring current in one junction, subtracts in other



2.6 SQUID Magnetometer

• In superconducting ring the magnetic flux is quantized, i.e because of wave nature of superconducting current (quantummechanics) the flux enclosed by the ring must be an integer number of the flux quantum $\Phi_0 = h/2e$


2. Measurement of magnetic field strength

2.6 SQUID Magnetometer

- Now suppose the external flux is further increased until it exceeds Φ_0 /2. Since the flux enclosed by the loop must be integer number of flux quanta, instead of screening the flux the SQUID now energetically prefers to increase it to Φ_0 . The screening current now flows in the opposite direction.
- \rightarrow screening current changes direction every time the flux increases by half integer multiples of Φ_0
 - \rightarrow critical current oscillates as a function of the applied flux

 \rightarrow voltage between A and B is function of applied magnetic field and a period equal to \varPhi_0



2. Measurement of magnetic field strength

2.6 SQUID Magnetometer

- In practise: SQUID is not directly contacted with magnetic source, device is rather linked to transformer coil to measure flux from small sample, i.e. sample magnetization
- SQUID magnetometer is high-sensitivity static fluxmeter
- Sensitivity: femto- to pico-Tesla
- Since SQUID requires low-T operation, it is usually used in conjunction with superconducting coil



Measurements to determine magnetic material parameters & properties

3

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

Measurements to determine magnetic material parameters & properties

3

General aspects

General aspects

Magnetic field H

Field produced by currents:

Lines of ${\cal H}$ are continuous and form closed loops



Field produced by magnetic poles:

Lines of H begin at north poles and end at south poles (here: $H_{applied} = 0$)



Demagnetizing field $H_{dem} = -N\overline{M}$: acts opposite to magnetization M that creates it

General aspects

Magnetic field H and Induction B

- $\boldsymbol{B} = \mu_0 (\boldsymbol{H} + \boldsymbol{M}) = \mu_0 (\boldsymbol{H}_{applied} \boldsymbol{H}_{dem} + \boldsymbol{M})$
- If $H_{applied} = 0$: H_{dem} is only field acting, and $B = -\mu_0 H_{dem} + \mu_0 M$
- $\mu_0 H_{dem}$ can never exceed $\mu_0 M$, i.e. flux density **B** inside magnet is always smaller than $\mu_0 M$, but in same direction



• Lines of **B** are continuous, from S to N inside magnet, outside $\mu_0 H = B$

Field produced by magnetic poles: Lines of H begin at north poles and

end at south poles (here: $\dot{H}_{applied} = 0$)





Demagnetizing field $H_{dem} = -N\overline{M}$: acts opposite to magnetization M that creates it

General aspects

Magnetic field H and Induction B

 Flux density of bar magnet is not uniform: B-lines diverge towards the ends → flux density is less than in center



• Exception: rotational ellipsoid:



Reason:

 H_{dem} is stronger near the poles





General aspects

Closed and open samples

Open sample

Internal field: $H_{in} = H_{applied} - N \cdot \overline{M}$



• Closed sample

Internal field: $H_{in} = H_{applied}$, N = 0



General aspects

Closed and open samples

Demagnetization effect

 \rightarrow Shearing of magnetizaton curve



Infinite sample or closed ring: unsheared hysteresis curve: N = 0, i.e. $H_{in} = H_{ext}$



Finite sample or open core: sheared hysteresis curve due to demagnetization effect (a higher H_{applied} is needed to achieve a given degree of M)

General aspects

Closed and open samples

Demagnetization effect

 \rightarrow Shearing of magnetizaton curve

- Internal field: $H_{in} = H_{applied} N \cdot M$
- Relevant for magnetic materials is the $M(H_{in})$ -curve, as it is independent of the sample shape
- If a magnetization curve was measured on a finite sample, it has to be re-sheared.





General aspects



General aspects

Demagnetizing factor Can only be calculated exactly for rotational ellipsoid

N along a-axis

 $N_{\rm a} + N_{\rm b} + N_{\rm c} = 1$ (*a*, *b*, *c*: main axes of ellipsoid)



Sphere: $a = b = c \rightarrow N_a = 1/3 = N_b = N_c$

General aspects

Demagnetizing factor

Numerical calculation for rectangular body

 $N_{\rm a} + N_{\rm b} + N_{\rm c} = 1$ applies



A. Hubert & RS, Magnetic Domains

General aspects

Demagnetizing factor

- Demagnetizing factor of compact bodies is often well approximated by that of inscribed ellipsoid
- Experimental determination of the demagnetization factor:
 - For every dc-field an ac-field of decreasing amplitude is superimposed (helps to over-come barriers in magnetization process)
 - Then approximately that magnetization is achieved, the demagnetizing field of which is equal to the applied field $[H_{in} = H_{applied} - N \cdot M = 0$ up to "knee" $\rightarrow M = (1/N) \cdot H_{applied}$
 - The initial slope of the magnetization curve is $dM/dH_{applied} = 1/N$
- If possible: avoid demagnetization effect by chosing proper sample geometry for magnetic measurement





 $N \approx 0$

Phase Theory and M(H) curve

Infinite or closed sample Finite sample $N = 0 \rightarrow H_{in} = H_{applied}$ $N \neq 0 \rightarrow \text{shearing} \rightarrow H_{\text{in}} = H_{\text{applied}} - N \cdot M$ Rotation $M/M_{\rm s}$ $M/M_{\rm s}$ "knee" 0.9 0.9 "knee" **H**_{ext} 0.8 0.8 $1/\sqrt{2}$ $1/\sqrt{2}$ \overrightarrow{H}_{ext} $H_{\rm ext}$ Mode III 0.6 0.6 0.5 0.5 $H_{\rm in} = 0$ **Wall displacement** 0.4 $H_{\rm in} = 0$ 0.3 0.3 $H_{\rm ext}$ Mode I 0.2 0.2 0.1 0.1 0 0 0.2 0.4 0.6 0.8 0.2 0.4 0.6 0.8 0 $H_{\text{applied}}/H_{\text{K}}$ \rightarrow $H_{\text{applied}}/H_{\text{K}} = H_{\text{in}}/H_{\text{K}}$

General aspects

Demagnetizing factor

- Demagnetizing factor of compact bodies is often well approximated by that of inscribed ellipsoid
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 $N \approx 0$

General aspects

Conclusion (demagnetization problematics):

The long-range nature of the demagnetizing field makes the measured property of any test specimen geometry-dependent

Demagnetizing field should be avoided when characterizing **soft** magnetic materials

Demagnetizing field can be tolerated when characterizing hard magnetic materials, provided it is accurately known and is possibly uniform

For finite, non-ellipsoidal samples the magnetization is nonuniform due to demagnetizing effects \rightarrow has to be considered when placing pick-up coil for inductive measurements

General aspects

Hysteresis curve:



General aspects

Hysteresis curve: B and M

- Difference between M(H) and B(H)
- Soft magnets: Fields involved in hysteresis loop are much smaller than corresponding magnetization values
 - $\rightarrow B \cong \mu_0 M$
 - \rightarrow difference between B(H) and M(H) negligible
- Hard magnets: H and M have comparable orders $\rightarrow B(H)$ significantly different from M(H)

$$B(H) = \mu_0 (H + M)$$





0.5

1.0

General aspects

Hysteresis curve: Anisotropy

- Magnetic anisotropy is defined as energy differences needed for saturation along different axes \rightarrow Magnetic anisotropy can be determined from M(H)-curve for single crystals by comparing magnetization curves along hard- and easy directions
- Example: cubic magnetocrystalline anisotropy (case of iron)

$$e_{\mathrm{Kc}} = K_{\mathrm{c}1} \cdot (m_1^2 m_2^2 + m_1^2 m_3^2 + m_2^2 m_3^2) + K_{\mathrm{c}2} m_1^2 m_2^2 m_3^2$$

 m_i = Magnetization components along cubic axes (direction cosine) K_{ci} = Anisotropy constants

$$m = [100]: e_{Kc} = 0$$

$$m = [110]: m_1 = m_2 = 1/\sqrt{2}$$

$$e_{Kc} = K_{c1} (1/2+0+0) = K_{c1}/4$$

$$m = [111]: m_1 = m_2 = m_3 = 1/\sqrt{3}$$

$$e_{Kc} = K_{c1} (1/9+1/9+1/9) + 1/27 K_{c2}$$

$$= 1/3 K_{c1} + 1/27 K_{c2}$$



Hysteresis curve: Ar

3. Magne

- Magnetic anisotropy is defined different axes → Magnetic ar single crystals by comparing r
- Example: cubic magnetocrysta

 $m = [100]: e_{Kc} = 0$

F1101

$$e_{\rm Kc} = K_{\rm c1} \cdot (m_1^2 m_2^2 + m_1^2 m_3^2)$$

 m_i = Magnetization com K_{ci} = Anisotropy consta



 $m_1 = 1/\sqrt{2} = \cos 45^\circ$

$$m = [110]: \quad m_1 = m_2 = 1/\sqrt{2}$$

$$e_{Kc} = K_{c1} (1/2+0+0) = K_{c1}/4$$

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11/2

General aspects

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- Example: cubic magnetocrystalline anisotropy (case of iron)

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 m_i = Magnetization components along cubic axes (direction cosine) K_{ci} = Anisotropy constants

- Limitations:
 - Hysteresis effects make the determination of the area ambiguous. Relying on the idealized magnetization curve offers fair solution to this problem
 - Non-ideal behaviour in approach to saturation. Internal stresses, inclusions and shape irregularities lead to a rounding of the magnetization curve. These effects depend on the magnetization direction because the magnetization deviations around such irregularities are influenced by anisotropy. The direct determination of the anisotropy from the magnetization curves is therefore often unreliable

General aspects

Hysteresis curve: Anisotropy

Singular Point Detection in polycrystals

- Detects singularities in magnetization curve of polycrystalline sample which are caused by singular contributions from certain grains
- Compare magnetization curves of uniaxial particles: There are field orientations for which curves are smooth, for others they show characteristic jumps

 first-order magnetization transitions
 h_⊥
- In polycrystalline sample: jumps of accordingly oriented grains will show up ______as singularities (maxima) in the second derivative of the magnetization curve, while the other grains only contribute to a smooth background ______

 \rightarrow Determination of anisotropy field H_{K}



General aspects

Hysteresis curve: Anisotropy

Singular Point Detection in polycrystals

- Detects singularities in magnetization curve of polycrystalline sample which are caused by singular contributions from certain grains
- Compare magnetization curves of uniaxial particles: There are field orientations for which curves are smooth, for others they show characteristic jumps
 = first-order magnetization transitions
- In polycrystalline sample: jumps of accordingly oriented grains will show up as singularities (maxima) in the second derivative of the magnetization curve, while the other grains only contribute to a smooth background
 - \rightarrow Determination of anisotropy field $H_{\rm K}$



Courtesy R. Grössinger, Vienna

General aspects

FORC: First Order Reversal Curve

• A FORC is measured by saturating sample in field H_{sat} , decreasing the field to a reversal field H_A , then sweeping field back to H_{sat} in a series of **equal** field steps H_B . The magnetization curve between H_A and H_B is a FORC



- The FORC distribution $\varrho(H_A, H_B)$ is defined as the mixed second derivative of the $M(H_A, H_B)$ - surface: $\varrho(H_A, H_B) = -\frac{\partial^2 M(H_A, H_B)}{\partial H_A \partial H_B}$
- $\varrho(H_{\rm C}, H_{\rm U})$ is plotted as contour- or 3D-plot







• $\varrho(H_{\rm C}, H_{\rm U})$ is plotted as contour- or 3D-plot



General aspects

FORC: First Order Reversal Curve $-\frac{\partial^2 M}{\partial H_A \partial H_B}$

- Example: Assemble of randomly orientated, noninteracting, uniaxial Single-Domain grains
- Central peak; switching of the magnetization at $H_{\rm switch}$
- Lower left-hand arm of the "boomerang": related to FORCs near the relatively abrupt positive switching field
- The right-hand arm of boomerang: related to more subtle contours, which are due to the FORCs having different return paths
- Negative region: related to sections of the FORCs where $H_{\rm B} < 0$

Muxworthy & Roberts, in: Encyclopedia of Geomagnetism and Paleomagnetism, Springer, 2007, Pages: 266 - 272



General aspects

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- Negative region: related to sections of the
- FORC distribution eliminates purely reversible components of magnetization process. Thus any non-zero *Q* corresponds to irreversible switching processes
- FORC thus provide insight into relative proportions of reversible and irreversible components of the magnetization process



General aspects FORC: First Order Reversal Curve

 $H_{\rm c}$ (mT)



Non-interacting SD grains, equally oriented: sharp peak, $H_{\rm C} = H_{\rm switch}$

Interacting SD grains: spreading in the HU direction

If the SD grains have a distribution of switching fields, this causes the FORC diagram to stretch out in $H_{\rm C}$ direction

General aspects

FORC: First Order Reversal Curve

Example: nanodot array of different dot diameter.
 Distinctly different reversal mechanisms, despite only subtle differences in the major hysteresis loops.





Courtesy Kai Liu, Davis Phys. Ref. B 75, 134405 (2007)

General aspects

Demagnetiziation

3 possibilities, to "demagnetize" a magnet (\overline{M} = 0) :

1. Thermal demagnetization

Heating above Curie temperature and cooling in absence of magnetic field







In principle any point within or on the hysteresis loop can be obtained by choosing the right field history Measurements to determine magnetic material parameters & properties

3

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods
Measurements to determine magnetic material parameters & properties

3

3.1 Magnetic measurements

- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

a) Inductive methods

Sample surrounded by coil, in which voltage is induced when magnetization of sample is changed or when sample is moved. Voltage is integrated \rightarrow signal proportional to magnetization

b) Magnetometric methods

For finite samples: demagnetizing field, which is proportional to mean magnetization ($H_{dem} = -N\overline{M}$), is measured

c) Optical magnetometry

Surface magnetization is measured by magneto-optic effect, useful for thin films where signal of inductive or magnetometric methods are too weak

a) Inductive methods

Measurement of closed circuit samples



a) Inductive methods

Measurement of closed circuit samples



Computer

a) Inductive methods Measurement of closed circuit samples

• Examples of closed samples



a) Inductive methods Air flux compensation

• $B = \mu_0 H + J \longrightarrow$

If J(H) is to be measured instead of B(H): Air flux compensation required to subtract effect of applied field

- Compensation coil arrangement: 2 coils with equal winding areas $A_1 \cdot n_1 = A_2 \cdot n_2$ ($A_{1,2}$: cross sectional area of coils, $n_{1,2}$: number of turns) are connected electrically in opposition \rightarrow difference signal is proportional to magnetization alone, i.e. without specimen in pick-up coil: no flux recorded by fluxmeter, with specimen in pick-up coil: fluxmeter reads ΔJ
- Two possibilities: (i) two identical coils arranged side by side; (ii) external layers of the winding of a coil can be connected in such a way that their winding area is equal and opposite to the core winding area



a) Inductive methods Air flux compensation

- Measurement of field strength:
 - Signal induced in compensation coil can also be used to measure the effective internal field
 - Maxwell's equations: tangential component of magnetic field must be equal on both sides of sample surface (if no current is flowing in sample surface)
 - → A coil placed close to the surface may therefore measure the internal field
 - With this technique the unsheared magnetization curve can be measured even for short samples
 - Alternative: Rogowski-Chattok coil





Magnet a) Induc lethods tracer Loop Highly sensitive commercial instrument to

inductively measure M(H) loops in soft -25 -10 -25 -25 -20 -8 magneticofilms

Jhb

- Helmholtz coils: field up to 100 mT •
- Frequency 1 10 Hz
- Alternative to Vibrating Sample • Magnetometer



Pick-up assemblies

asurements

gnetic films

MESA http://www.shbinstruments.com



a) Inductive methods (Quasi-)static magnetization

- Quasistatic *M*(*H*) measurement: rate of magnetization d*B*/d*t* and time for complete hysteresis cycle have to be low enough to eliminate all dynamic effects (like eddy currents, relaxaton processes etc.)
- Quasistatic loop is narrower than AC loop;
- Quasistatic coercivity is always lower than dynamic coercivity



a) Inductive methods Dynamic magnetization

- AC magnetization at low excitation level:
 - Field amplitude below coercive field (Rayleigh region)
 - Relationship between AC flux density and AC field strength can be represented by ratio factor (permeability) and phase angle (magnetic loss angle due to eddy currents)
 - Can be described in terms of classical eddy current theory



a) Inductive methods Dynamic magnetization

- AC magnetization at high excitation level:
 - AC excitation into region of maximum permeability and up to saturation
 - Severe distortions of magnetization due to non-linear behaviour of ferromagnetic material (S-like or rectangular hysteresis loops). Reason:
 - At high excitation level: material is subjected to rapid changes of H(t) or B(t)
 - Local magn. flux density cannot follow changes due to eddy curents
 - Consequence: Magnetization curve depends on frequency and mode of excitation
 - 2 modes of dynamic magnetization:
 - Voltage-controlled magnetization: induced voltage is controlled to be sinusoidal (by feedback loop) \rightarrow sinusoidal flux density $B(t) \rightarrow$ magnetizing current I(t) becomes dependent. Recommended as IEC standard
 - Current-controlled magnetization: magnetizing current is controlled to be sinusoidal (by high-impedence power source) \rightarrow sinusoidal field strength $H(t) \rightarrow U(t)$ and B(t) become dependent.



a) Inductive methods Dynamic magnetization

high excitation level



Controlled sinusoidal flux density B(t) $U(t) = (-) n_2 \cdot A_{\rm Fe} \frac{\mathrm{d}B}{\mathrm{d}t}$ \rightarrow Induced voltage U(t) also exhibits sinusoidal waveform $\rightarrow H(t)$ heavily distorted Flux density B in T 0.8 0.6 0.4 B(H)0.2 0.0 -0.2 -0.4 -0.6 $f = 50 \, \text{Hz}$ -0.8 -1.0-200 400 600 800 -800 -600 -400 -200 0 Field strength H [A/m]



Controlled sinusoidal field strength H(t) \rightarrow Step-wise characteristics of B(t). Abrupt changes of B(t) are traversed in short time interval \rightarrow Spikes in induced voltage U(t) \rightarrow Large eddy

currents, sheared loop



a) Inductive methods Loss measurement

- Wattmeter method (e.g.)
 - Measures core loss (not copper loss)
 - Losses are measured at certain maximum flux density and given frequency
 - Total weight of sample is recorded, and losses are reported in W/kg



a) Inductive methods Loss measurement

Energy loss



Frequency





Transformer sheet

a) Inductive methods Loss measurement





a) Inductive methods Loss measurement





Frequency increases 10 \longrightarrow 100 Hz



a) Inductive methods Extraction Method

 Based on flux change in pick-up coil when sample is extracted from coil, or when specimen and pick-up coil together are extracted from field

Total flux through pick-up coil:

$$\Phi_1 = BA = \mu_0 (H + M) A = \mu_0 (H_{applied} - NM + M) A$$

If sample is removed from pick-up coil, the flux through the coil becomes:

 $\Phi_2 = \mu_0 H_{applied} A$ A: specimen or pick-up coil area

Fluxmeter will record a value proportional to flux change:

 $\Phi_1 - \Phi_2 = \mu_0 (1 - N) MA$

- Extraction method measures M directly, rather than B
- Vibrating sample magnetometer: may be regarded as partial extraction method



- Sample placed inside magnet and vibrated perpendicular to field direction (frequ. ~ 100 Hz, vibration ampl. ~ 0.1 mm)
- Oscillating magnetization of moving sample \rightarrow induces alternating voltage in pick-up coil, whose magnitude is proportinal to M_{sample} : $U_{\text{ind}} = const \cdot V \cdot M_{\text{sample}}$ (V: sample volume)
- The pick-up signal is amplified with lock-in amplifier and compared with the signal induced in a pair of reference coils by a permanent magnet or by some variable capacitor setup (only sensitive to vibration frequency)
- Strong external fields can be applied (superconducting magnets for hard magnetic materials)
- Since sample is well-separated from the pick-up coils, it can be surrounded by cooling or heating devices
- The sample magnetization is static in the VSM, so that no eddy current effects have to be considered



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a) Inductive methods

Vibrating Sample Magnetometer (VSM)

16

solenoid

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linear motor supercoducting Courtesy Quantum D

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a) Inductive methods

- Direct method. Ideally, no calibration would be needed to derive the magnetization of the sample if pick-up coil geometry and sample volume are known and if magnetic field could be generated by a simple air coil
- However: for electromagnets the pole material interacts with the measuring process: "mirror images" of the sample are formed by the presence of soft magnetic iron yokes
- \rightarrow Mirror images also induce voltage in pick-up coil
- Strength of mirror images depends on permeability of iron yoke that in turn depends on the induction level in magnet
- \rightarrow VSM must be calibrated by replacing sample by Ni sample with accurately known saturation magnetization \rightarrow determines *const* in $U_{\text{ind}} = const \cdot V \cdot M_{\text{sample}}$



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a) Inductive methods

- VSM measures magnetic moment and therefore magnetization M whereas fluxmeter methods measure flux density B
- VSM is best method to measure the saturation magnetization $M_{\rm s}$ of any material because high field can be applied to reach saturation
- VSM less useful for measurement of other parameters of magnetization curve in soft magnetic materials because of demagnetization effects (real field unknown).
 Exception: thin films. For high-anisotropy or hard magnetic materials, however, the VSM is the preferred instrument for many kinds of magnetic measurements
- Sensitivity: 10^{-5} emu = 10^{-8} Am² \rightarrow small samples (< 1 gramm)
- Pick-up coil arangements to measure longitdinal and transverse magnetization components
- SQUID magnetometer: high-sensitive variant of VSM. Pick-up signal transformed to SQUID device outside magnet



a) Inductive methods

Sample surrounded by coil, in which voltage is induced when magnetization of sample is changed or when sample is moved. Voltage is integrated \rightarrow signal proportional to magnetization

b) Magnetometric methods

For finite samples: demagnetizing field, which is proportional to mean magnetization ($H_{dem} = -N\overline{M}$), is measured

c) Optical magnetometry

Surface magnetization is measured by magneto-optic effect, useful for thin films where signal of inductive or magnetometric methods are too weak

b) Magnetometric measurements

- Magnetometer measures dipolar field generated by magnetized sample with the help of field detection device (e.g. Hall probe)
- In shown arrangement the difference signal of the two probes is proportional to the magnetic moment of the sample, and insensitive to the driving field
- Probes must be placed sufficiently for away from sample, so that only its dipolar field is detected \rightarrow samples should be small and short, but can be of any shape \rightarrow hard and high-anisotropy materials better suited than soft magnetic materials where demagnetization will dominate the intrinsic properties of short samples
- Advantages: (i) any sample shape, (ii) arbitrarily slow magnetization processes can be followed, (iii) sample can be easily exposed to various environmental conditions such as high or low temperature or mechanical stress.



c) Optical magnetometer Magneto-optical Kerr effect

 $\boldsymbol{D} = \boldsymbol{\varepsilon} \boldsymbol{E} = \boldsymbol{\varepsilon} \begin{pmatrix} 1 & -i Q m_3 & i Q m_2 \\ i Q m_3 & 1 & -i Q m_1 \\ -i Q m_2 & i Q m_1 & 1 \end{pmatrix} \boldsymbol{E}$

 $= \varepsilon E + i \varepsilon Q m \times E$

- E: electric vector of light wave
- D: dielectric displacement vector

(= vector of light after reflection)

- *m*_i: components of magnetization vector (cubic crystal)
- $\boldsymbol{\mathcal{E}}$: dielectric tensor
- Q: material constant ($\sim M_s$, complex, determines strength of rotation)

c) Optical magnetometer

Magneto-optical Kerr effect

$$D = \varepsilon E = \varepsilon \begin{pmatrix} 1 & -iQ m_3 & iQ m_2 \\ iQ m_3 & 1 & -iQ m_1 \\ -iQ m_2 & iQ m_1 & 1 \end{pmatrix} E$$
$$= \varepsilon E + i\varepsilon Q m \times E \longrightarrow \text{concept of Lorentz force}$$

mxE

- E: electric vector of light wave
- **D** : dielectric displacement vector
 - (= vector of light after reflection)
- *m*_i: components of magnetization vector (cubic crystal)
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3.1 Magnetic Measurements

c) Optical magnetometer Magneto-optical Kerr effect



The Kerr effect causes a rotation of light, which is proportional to the magnetization component parallel to the reflected light beam

3.1 Magnetic Measurements

c) Optical magnetometer

- Magneto-optical Kerr effect is linear function of magnetization and therefore well-suited for magnetometry
- For non-transparent material optical magnetometry makes sense only for thin films for which surface magnetization is representative
- Advantages: (i) direct, (ii) quasi-static and dynamic measurements, (iii) Space-resolved measurements are possible by scanning over the surface. (iv) Optical measurements can be performed on-line during preparation or treatment of a material for example inside vacuum chamber
- Noise suppression: feed split-off part of laser light as reference signal into amplifier. If polarization of light is modulated by a spinning analyser or electrooptical device, the magnetic signal can be detected by a lock-in amplifier, thus achieving virtually unlimited sensitivity



3.1 Magnetic Measurements

b) Optical magnetometer

• Polar Kerr magnetometer (P-MOKE)

Polar Sample Sample Sample Detachable right angle polar Kerr lens

NANOMOKE3® http://www.lot-qd.de

Longitudinal



- Use of transverse Kerr effect (T-MOKE)
 - Polarizer set parallel to the plane of incidence and analyser omitted
 - *M*-component perpendicular to the plane of incidence causes variation of the reflected intensity, which can be detected electronically
 - Fits nicely into electromagnet



Measurements to determine magnetic material parameters & properties

3

3.1 Magnetic measurements

- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

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Principle: Measurement of mechanical forces on magnetic sample

Two possibilities:

- A uniform field H, acting on uniformly magnetized sample of magnetization M and volume V, generates a mechanical torque $T_m = \mu_0 V H \times M$
- Gradient of non-uniform field generates a mechanical force $F_m = \mu_0 V \operatorname{grad}(M \cdot H)$

a) Torque magnetometer

Most direct method to measure anisotropy

b) Field gradient mathods

Faraday Balance and Alternating Gradient Magnetometer





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Faraday Balance and Alternating Gradient Magnetometer

a) Torque magnetometer

0

 $-0.5 K_1$

- Torque measurements offer most direct methods for measuring anisotropies
- Requires uniform, single-crystalline samples, preferably of spherical or disk shape
- Example: crystal with cubic anisotropy:

Anisotropy energy:

$$E = K_0 + K_1 \sin^2\theta \,\cos^2\theta,$$

Torque (assumption: $M_s \parallel H$):

$$L = -\frac{dE}{d\theta} = -K_1 \sin 2\theta \cos 2\theta$$
$$= -\frac{K_1}{2} \sin 4\theta.$$

Anisotropy constant can be measured by torque measurement



a) Torque magnetometer

Example: Torque meter with active sensing

- Sample hung from sensitive torsion fiber, placed in electromagnet that can be rotated
- Torque coil, placed in field of permanent magnet. Current through torque coil: coil experiences torque proportional to current
- Sensing circuit (light beam, mirror, photocell) provides feedback signal that drives a current through the torque coil to balance the anisotropy torque of sample
- Sample can be held at any angle to the field of the electromagnet
- Value of current through torque coil is proportional to torque on sample



- Non-spherical body in homogeneous field will rotate till its long axis is parallel to field (compass needle)
- Field gradient: Field is stronger at north pole than at south pole \rightarrow net force F_x to right, with m = magnetic moment and v = volume of body
- Force $\sim M$
- Body will move toward region of greater field strength (to right)





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- Measures static force on sample in magnetic field gradient
- Uniform field is generated by electromagnet, and the gradient field is produced by an additional coil-set, optimized for a uniform magnetic gradient along y-axis
- If sample is mounted elastically, it is displaced by force
- Force can be detected and compensated by a calibrated electromagnetic counter-force.
 Compensation current is measure of force.
 Only quantity needed: sample volume
- Highly sensitive, can be applied to all kinds of magnetic substances
- In ferromagnetism it is best suited to measure the saturation magnetization with high precision



b) Field gradient methods Alternating Gradient Magnetometer (AGM)

- AGM (or Vibrating Reed Magnetometer) resembles superficially the VSM
- VSM: sample agitated mechanically and electric signal is derived from motion.

AGM: magnetically excited signal is recorded

- Sample mounted on elastic cantilever or "reed", which is excited into resonant vibration by alternating gradient field (produced by gradient coils in addition to dc magnet) by chosing resonance frequency
- Vibration is recorded by piezoelectric pick-up system: generates voltage proportional to vibration amplitude (proportional to force) = proportional to sample magnetic moment
- Sensitivity: 10⁻⁶ emu = 10⁻⁹ Am² → higher than
 VSM



b) Field gradient methods

Alternating Gradient Magnetometer (AGM)





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Ferromagnetic Resonance (FMR)

- FMR is dynamic measurement method at microwave frequency (GHz-regime, order of Lamor frequency)
 - Because of high-frequency alternating magnetic field: eddy current shielding in metals is nearly complete (penetration depth of field ~ 200 nm)
 - \rightarrow resonance methods are not applicable to bulk metallic samples
 - → can only be applied to non-conducting oxidic materials, thin films, and powdered materials
- Typical FMR resonance experiment:
 - Sample magnetized in strong static field $H_{\rm ex}$ to enforce uniformly magnetized state
 - To induce resonance phenomenen: alternating field with fixed GHz-frequency is superimposed at right angle to magnetization direction → stimulates precession of magnetization vector
 - The static field amplitude H_{ex} is swept till resonance is achieved at $H_{ex} = H_{res}$ (sweeping of field is easier than sweeping microwave frequency)



Ferromagnetic Resonance (FMR)

Resonance frequency:

$$\omega_{\rm res} = \gamma H_{\rm res} \quad \text{with} \quad \gamma = \mu_0 ge/2m_{\rm e}$$

$$H_{\rm res} = \sqrt{\left[\frac{2K_{\rm u}}{\mu_0 M_{\rm s}} + H_{\rm ex} + M_{\rm s} \left(N_{\rm b} - N_{\rm a}\right)\right] \left[\frac{2K_{\rm u}}{\mu_0 M_{\rm s}} + H_{\rm ex} + M_{\rm s} \left(N_{\rm c} - N_{\rm a}\right)\right]}$$

$$Anisotropy \quad \text{External} \quad \text{Demagnetizing} \quad \text{field} \quad \text{field} \quad \text{Magnet}$$

• If M_s and N_i are known \rightarrow anisotropy K_u can be derived from measuring $H_{\rm res}$



Ferromagnetic Resonance (FMR)

• Based on LLG equation:

$$\frac{\mathrm{d}M}{\mathrm{d}t} = -\gamma_0 \left[M \ge H_{\mathrm{eff}}\right] + \frac{\alpha}{M_{\mathrm{s}}} \left[M \ge \frac{\mathrm{d}M}{\mathrm{d}t}\right]$$

Desribes (damped) precession of M around effective field $H_{\rm eff}$, caused by gyrotropic reaction of magnetic moment due to its angular momentum

- If the precession is uniform (does not depend on the position in sample): ferromagnetic resonance
- At higher frequencies, non-uniform precession modes may be excited:
 - If their wavelength is comparable with sample size: magnetostatic modes
 - Resonance phenomena at shorter wavelengths depend on the exchange stiffness constant and are called spin-wave modes
 - Finally, there are surface modes of magnetic resonance which can be excited for example by light instead of an alternating field. Then spectroscopy replaces the standard inductive detection methods



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\rightarrow Lecture of B. Hillebrands

H_{eff}

M

 $M \times H_{\rm eff}$

Ferromagnetic Resonance (FMR)

- FMR experiment:
 - Microwave field is generated by Klystron or Gunn diode and conducted to sample by wave guide (hollow metal tube)
 - Sample centered in microwave cavity (closed hollow metal structure), located in electromagnet

 \rightarrow Microwave frequency fixed and determined by klystron and cavity. Alternativly sample can be placed on micro-stripline

- Incident microwave signal couples to sample and is partially absorbed in dependence of field strength $H_{\rm ex}$





- If resonance condition is fulfilled \rightarrow max. absorption of microwave power by sample
- Crystal detector measures reflected microwave signal. This signal is input into lock-in amplifier where it is compared with reference signal
- Output of lockin vs. external field: corresponds to derivative of absorption curve, i.e the change of absorbed intensity I as function of H_{ex} : dI/dH_{ex}

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Ferromagnetic Resonance (FMR)

- Resonance field $H_{\rm res}$ and half power line width ΔH can be determined
- $H_{\rm res} \rightarrow$ magnetic anisotropy
- $\Delta H \rightarrow$ relaxation
- Intensity $\rightarrow M_s$





B. Heinrich et al., PRL 59, 1756 (1987)

Spinwave Resonance

Light Scattering experiments

Spinwave Resonance

Light Scattering experiments

\rightarrow Lecture of B. Hillebrands

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Magnetostriction

- Example: cubic crystal (iron) with 4 domain phases in ground state \rightarrow no net-magnetization
- Each domain elongates crystal along M-direction \rightarrow cubic lattice gets tetragonally distorted
- Application of magnetic field, saturation \rightarrow elongation of total crystal
- Relative length change $\Delta l / l = \lambda_s$ $\lambda_s =$ magnetostriction coefficient
- $\lambda_s > 0$: elongation in magnetization direction, $\lambda_s < 0$: compression
- Note: 180°-domains are elongated along same axis
- λ for iron: 20·10⁻⁶ \rightarrow very small effect



Magnetostriction measurement, remark

 Every direct determination of magnetostriction constant requires measurement of length change between two different saturated states — usually parallel and perpendicular to measuring direction. Experiment with field applied along only one axis of crystal yields no useful information on magnetostriction constants, because then only some arbitrary demagnetized state and the saturated states are compared



 L_0 : length of hypothetic non-magnetic state

Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Indirect methods: stress sensitivity of a suitable magnetic property is analysed, more suitable for thin films and wires

Example: magnetization curve and resonance measurements, if performed as function of external stress, can be evaluated in terms of magneto-elastic coefficients



Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Direct measurements: evaluate elongation of a magnet depending on the magnetization direction, preferred for bulk samples of sufficient size

Strain Gauges

- Plastic foil on which structured metal films act as sensors, cemented on sample
- Based on (small) change of el. resistance by elongation, measured with bridge circuit
- Strain gauge can be applied locally on favourable small region of single crystal or even on grain in a coarse-grained sample. Active area down to 1 mm²
- It is always advisable to apply strain gauges on both sides of sample, and to connect them in series to avoid influence from sample bending induced by one-sided heating by the measuring current


3.4 Dilatometric Measurements

Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - Direct measurements: evaluate elongation of a magnet depending on the magnetization direction, preferred for bulk samples of sufficient size

Dilatometers

- Capacitive sensors, optical interferometers, tunnelling sensor, piezo sensor...
- With normal samples of centimetre dimension a resolution in the nanometre range is required



3.4 Dilatometric Measurements

Magnetostriction measurement

- Saturation magnetostriction constants can be determined both directly or indirectly:
 - **Direct measurements**: evaluate elongation of a magnet depending on the • magnetization direction, preferred for bulk samples of sufficient size

Cantilever for films

- Magnetostrictive bending of a sample-substratecomposite in magnetic field is optically detected as measuring signal by reflected laser beam, a quadrant detector and lock-in technique
- Sample esposed to rotating saturation field •
- Deflection difference $d_{\rm f}$ of free end of cantilever for • longitudinal and transverse magnetization:

$$d_{\rm f} = d_{\parallel} - d_{\perp} = \frac{3D_{\rm f}L^2}{D_{\rm s}^2} \frac{E_{\rm f}(1+\nu_{\rm s})}{E_{\rm s}(1+\nu_{\rm f})} \cdot \frac{3}{2}\lambda_{\rm s}\sin^2\vartheta$$

 $E_{\rm x}$ and $\nu_{\rm x}$: Young's moduli and Poisson's ratios of film and substrate, θ : magnetization angle ($\theta = 0$ for magnetization along cantilever)



Laser

position sensitive

detector

Measurements to determine magnetic material parameters & properties

- 3.1 Magnetic measurements
- 3.2 Mechanical measurements
- 3.3 Resonance techniques
- 3.4 Dilatometric measurements
- 3.5 Domain methods

Measurements to determine magnetic material parameters & properties

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Magnetic energies

Energy term	Coeff	icient	Definition	Range
Exchange energy	A	[J/m]	Material constant	$10^{-12} - 2 \cdot 10^{-11} \text{ J/m}$
Anisotropy energies	$K_{\rm u}, K_{\rm c}$.	[J/m ³]	Material constants	$\pm (10^2 - 2 \cdot 10^7) \text{ J/m}^3$
External field energy	$H_{\rm ex} J_{\rm s}$	[J/m ³]	H_{ex} = external field J_{s} = saturation magnetization	Open, depending on field magnitude
Stray field energy	K _d	[J/m ³]	$K_{\rm d} = J_{\rm s}^2 / 2 \ \mu_0$	$0 - 3 \cdot 10^6 \text{ J/m}^3$
External stress energy	$\sigma_{\rm ex}\lambda$	[J/m ³]	σ_{ex} = external stress λ = magnetostriction constant	Open, depending on stress magnitude
Magnetostrictive self energy	$C \lambda^2$	[J/m ³]	C = shear modulus	$0 - 10^3 \text{ J/m}^3$

Principle:

Under favourable circumstances material constants may be derived directly from observed domains. Such approach requires an equilibrium situation for which a reliable theoretical treatment is possible.

Example: Surface domain width in bulk uniaxial crystals



Example: Surface domain width in bulk uniaxial crystals

NdFeB magnet, c-axis perpendicular

um

For sufficiently thick crystals: surface domain width $W_{\rm s}$ constant, independent of sample

dimensions, depends only on wall energy γ_{W} and stray field energy constant $K_1 = \mu_0 M_s^2 / 2$: $W_{\rm s} = 108 \ \gamma_{\rm W}/K_{\rm d}$ $\gamma_{\rm W} = \pi \sqrt{A/K_{\rm u}}$ length sections

4. Domain scale measurements (Magnetic Imaging)

5. Magnetization curve

5. Magnetization curve

Η

Magnetic Microstructure Analysis

1. Atomic Foundation

Spin

Descriptive levels of magn. materials

5. Magnetization curve

H

M

Magnetic Microstructure Analysis

Atomic Foundation

Descriptive levels of magn. materials M

5. Magnetization curve

H

Magnetic Microstructure Analysis

Atomic Foundation

Descriptive levels of magn. materials

 $m = M/M_{\rm s}$

5. Magnetization curve

H

M

Magnetic Microstructure Analysis

Spin

Co₂₇Sm₇₃ amorphous film (thickness 200 nm)

Sample: F. Magnus and B. Hjörvarsson, Uppsala University (unpublished)

Biquadratic coupling in multilayers

Fe (30 nm) Cr (1.6 nm) Fe (30 nm)

M. Rührig, RS, et al., Phys. Stat. Sol. 125 (1991)

Domain Shift Register Devices

Bubble Memory

http://commons.wikimedia.org/wiki/ How_bubble_memory_works

Race Track Memory

Kerr-movie of Co/Ni PMA multilayer courtesy S. Parkin, IBM

Sensitivity of imaging methods

- $B = \mu_0 (H + M) \quad (H = H_{ext} + H_{stray})$ div B = 0 \downarrow div $H_{stray} = - \operatorname{div} M$
- Sensitive to $H_{\rm stray}$

Sensitive to M

- \cdot Sensitive to **B**
- Sensitive to distortions

- Bitter technique
- Magnetic force microscopy
- Hall probe microscopy
- Magneto-optical microscopy
- X-ray spectroscopy
- Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering

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History: first imaging of domains by F. Bitter, 1931)

Cobalt

Principle

- Magnetic colloid: Magnetite particles (diameter about 10 nm) in water
- Accumulation in stray field at sample surface

Sensitivity

- Reversible agglomeration in weak magnetic field
 - \rightarrow Increase of volume, elongated shape
 - \rightarrow Large susceptibility
 - \rightarrow Large sensitivity to stray fields in order of a few 100 A/m

Agglomeration in magnetic field (560 A/m)

Sensitivity

Increase of sensitivity in weak perpendicular field

Domain imaging in soft magnetic materials

Without auxiliary field

With perpendicular field

Dry colloid technique

Allowing colloid to dry on surface Adding agent

- \rightarrow Strippable film
- \rightarrow Imaging in electron microscope

Ba-Ferrite particles (courtesy K. Goto, Sendai)

Dry colloid technique:

Static domain observation on rough, 3-dimensional surfaces at high resolution of some 10 nm

Dry colloid technique

Allowing colloid to dry on surface Adding agent

- \rightarrow Strippable film
- \rightarrow Imaging in electron microscope

CoCr recording medium (courtesy J. Simsová, Prague)

Dry colloid technique:

Static domain observation on rough, 3-dimensional surfaces at high resolution of some 10 nm

Visible and invisible features

V-lines

Bitter image

Kerr image

Visible and invisible features

Kerr image

Ψ -lines

Bitter image

Kerr image

Bitter image

Visible and invisible features

Ψ -lines

Bitter image

Kerr image

Bitter image

Toner powder emulsion

Laser printer toner + water + household detergent

Toner powder emulsion

Laser printer toner + water + household detergent

Toner powder emulsion

Laser printer toner + water + household detergent

Transformer steel (courtesy S. Arai, Nippon steel)

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		<u> </u>
- Spin-off of scanning tunnelling microscope
- Tip-shaped probe at free end of cantilever (= flexible beam). Tip position detected (e.g.) by optical interference between tip of a fibre and cantilever



- 2 modes:
 - Static mode: MFM is run at constant force (equivalent to constant deflection of the cantilever) and the height necessary to obtain this state is used as the imaging information
 - Dynamic mode: Cantilever is operated at frequency close to its mechanical resonance, and change in resonance amplitude or shift in phase due to stray field interaction are detected. Since a magnetic force gradient is equivalent to an additional contribution to the spring constant of the cantilever, profiles of constant force gradient are recorded this way

- Spin-off of scanning tunnelling microscope
- Tip-shaped probe at free end of cantilever (= flexible beam). Tip position detected (e.g.) by optical interference between tip of a fibre and cantilever



- 2 modes:
 - Static mode: MFM is run at constant force (equivalent to constant deflection of the cantilever) and the height necessary to obtain this state is used as the imaging information

Data track on hard disk



Co elements

(111) Fe surface





Conventional interpretation of MFM: $F = -\partial E_{inter}/\partial z$; $\partial F/\partial z = -\partial E_{inter}^2/\partial z^2$

$$E_{\text{inter}} = -\int_{\text{tip}} J_{\text{tip}} \cdot H_{\text{sample}} \, dV = -\int_{\text{sample}} J_{\text{sample}} \cdot H_{\text{tip}} \, dV$$

$$H_{\rm tip} = - \operatorname{grad} \overline{\Phi}_{\rm tip}$$
, partial integration

$$\Phi_{\rm tip}$$
 = tip potential



Alternative interpretation Hubert, Rave, Tomlinson: Phys. Stat. Sol. B204, 817 (1997)

$$E_{\text{inter}} = \int \sigma_{\text{sample}} \Phi_{\text{tip}} dS + \int \rho_{\text{sample}} \Phi_{\text{tip}} dV$$
surface
$$\int \sigma_{\text{sample}} \Phi_{\text{tip}} dS + \int \rho_{\text{sample}} \Phi_{\text{tip}} dV$$

 $\sigma_{\text{sample}} = n \cdot J_{\text{sample}}$ (surface charge) $\rho_{\text{sample}} = -\operatorname{div} J_{\text{sample}}$ (volume charge)

Force
$$F = -\frac{\partial E_{\text{inter}}}{\partial z} = -\int (\frac{\partial \sigma}{\partial z} \Phi + \sigma \frac{\partial \Phi}{\partial z}) dS - \int (\frac{\partial \rho}{\partial z} \Phi + \rho \frac{\partial \Phi}{\partial z}) dV$$

for weak interaction
 $\approx -\int \sigma \frac{\partial \Phi}{\partial z} dS - \int \rho \frac{\partial \Phi}{\partial z} dV$
Force $\frac{\partial F}{\partial z} = -\frac{\partial E_{\text{inter}}^2}{\partial z^2} \approx -\int \sigma \frac{\partial^2 \Phi}{\partial z^2} dS - \int \rho \frac{\partial^2 \Phi}{\partial z^2} dV$



In the limit of weak interaction: MFM is Charge Microscopy

Charge contrast



Charge contrast



FeTnN element (30 nm) (courtesy J. Miltat)





Simulated charge distribution A. Hubert, W. Rave, S. Tomlinson: Phys. Stat. Sol. B 204, 817 (1997)

Charge contrast



Charge contrast is inverted when tip polarity is inverted

Induced charges: susceptibility contrast



→ Tip induces charges of opposite polarity in each case
→ Always attractive interaction (independent of tip polarity)
→ Strength of attraction depends on local susceptibility

Charge & susceptibility contrast

E. Zueco et al.:

JMMM 190, 42 (1998)

Stronger

Weaker

attraction

attraction

- Charge contrast is inverted by inversion of tip magnetization,
- Suscept. contrast: not inverted
- → Separation of charge and susceptibility contrast by difference and sum images

NdFeB twin boundary



Kerr image



MFM: charge contrast







Susceptibility contrast

Depth sensitivity



Fe whisker

111 · ` **** | | **|** |

Asymmetric vortex wall

E. Zueco et al., JMMM 196, 115 (1999)

3. Hall-Probe Microscopy

56 µm



NdFeB crystal

Together with J. McCord and U. Wolff, IFW

Sensitivity of imaging methods

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Difference image technique







Domains on (100)-FeSi sheet

Quantitative Kerr microscopy

Domains in magnetostriction-free amorphous ribbon

as-quenched state

after annealing in rotating field





5 µm

MOKE-Magnetometry and domains













Depth sensitivity of Kerr microscopy



Co/Si/GdCo trilayer

Sample: A. Svalov and G. Kurlyandskaya, Ekaterinburg Imaging: together with L. Lokamani, Dresden (unpublished)



















Mixed Kerr signal

GdCo layer

Co layer

50 µm



Mixed Kerr signal

GdCo layer



50 µm

Layer-selective Kerr microscopy



R. S., R. Urban, D. Ullmann, H. L. Meyerheim, B. Heinrich, L. Schultz, J. Kirschner, PRB 65, 144405 (2003)

Time-resolved (stroboscopic) imaging

illumination intensity and repetition rate are limited

- \rightarrow no single-shot imaging possible
- → accumulation of large number of independent events necessary (at fixed time delay)
- → requires repetitive magnetization processes !!



probing with defined time delay



periodic magnetic field excitation
4. Magneto-optical Kerr-Microscopy

Time-resolved (stroboscopic) imaging

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probing with defined time delay



periodic magnetic field excitation

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- → requires repetitive magnetization processes !!



probing with defined time delay



periodic magnetic field excitation



4. Magneto-optical Kerr-Microscopy



Magnetic history



Magnetic history

Indicator film technique: stray field imaging





Metallographic contrast



With indicator film





Bulk NiMnGa single crystal (shape memory material, does not show direct Kerr contrast)

Indicator film technique: stray field imaging

Grain oriented electrical steel:



Direct Kerr contrast (sample polished) MOIF contrast (sample polished) MOIF contrast (with insulation coating)

Domain contrast even through coating

Indicator film technique: stray field imaging

Grain oriented electrical steel:



Н

MOIF contrast (with insulation coating)

Magnetic Pole contrast at grain boundaries

Indicator film technique: stray field imaging

Direct image of surface



Rail track with crack

MOIF image



Imaging of defects for non-destructive testing

Together with G. Y. Tian, Chengdu

X-Ray Magnetic Circular Dichroism (XMCD)

XMCD: Absorption of circularly polarized X-rays depends on orientation of magnetization M with respect to helicity of the X-rays, change of sign by reversing M

X-Ray Magnetic Circular Dichroism (XMCD)

XMCD: Absorption of circularly polarized X-rays depends on orientation of magnetization M with respect to helicity of the X-rays, change of sign by reversing M

Physical origin: If energy of absorbed photon exceeds binding energy of an inner core level (e.g. $p_{1/2}$ and $p_{3/2}$ states, separated by spin-orbit coupling)

→ Transition into unoccupied spin-split states above Fermi level (e.g. into 3d band)

Initial states are well defined inner-core levels

 \rightarrow XMCD is element selective

Fermi's golden rule: transition probability of absorption process is related to density of unoccupied states, which are different for minority and majority bands due to exchange interaction

 \rightarrow X-MCD signal is proportional to magnetic moment of absorbing atom \rightarrow Sensing of magnetization of sample



X-Ray Magnetic Circular Dichroism (XMCD)



XMCD effect is localized around L_2 (transition from $2p_{1/2}$ core level to unoccupied 3d states) and L_3 (transition from $2p_{3/2}$ core level) absorption edges



XMCD detects the difference in absorption for the projection of the sample's magnetization onto the propagation direction of circularly polarized X rays. XMCD distinguishes between magnetization parallel and antiparallel to the light **propagation** direction (in-plane magnetization at perpendicular incidence: no XMCD)

5. X-Ray Spectroscopy 5.1 Transmission X-Ray microscopy Condenser zone plate Plane Applied mirror magnetic field **ALS Bending** Magnet Pinhole Image Object Micro Sample zone stage plate Soft x-ray sensitive Si_3N_4 membrane, 0.1 mm x 0.1mm, 35 nm thick CCD mm 0.3

Large absorption of soft X-rays (energy < 1 keV):

2 mm

film thickness < 100 nm

Circularly polarized

X-rays

thin substrates (Si₃N₄)

5.1 Transmission X-Ray microscopy

Switching of Fe/Gd multilayered dots



Courtesy P. Fischer, Th. Eimüller

5.1 Transmission X-Ray microscopy

Intensity profile across the boundary of a magnetic domain in an amorphous GdFe layer showing a lateral resolution of less than 15 nm



Courtesy P. Fischer

Courtesy P. Fischer, Th. Eimüller

5.1 Transmission X-Ray microscopy



M,



 M_4

 L_2

1µm



Gd

MTXM images of an amorphous Gd₂₅Fe₇₅ layer recorded at the spin- orbit-coupled Fe L₃ (a) and L₂ (b) as well as at the Gd M₅ (c) and M₄ (d) absorption edges

 Contrast inversion: magnetic moments on Cd and Fe couple antiparallel

Courtesy P. Fischer

5.1 Transmission X-Ray microscopy

In-plane imaging

Dichroic contrast: given by projection of M on photon propagation direction. In-plane imaging by tilting the sample (30°):





1 µm



5.1 Transmission X-Ray microscopy



Excitation of vortex structure in ac field (frequency 250 MHz, amplitude 0.1 mT). After a 4 ns 'single period' burst (amplitude 1.5 mT) the vortex core polarity is inverted B. Van Waeyenberge et al., Nature 444, 461 (2006)

5.2 X-ray Photoemission Electron Microscopy (X-PEEM)



- Excitation of core electron into empty valence state by incoming X-ray
- Recombination (e.g.) by Auger decay

Courtesy H.Ohldag



- nA
- Inelastic scattering of original photoelectron and auger electron
 leads to emission of secondary electrons
- Electron yield ~ X-ray absorption coefficient
- Probing depth ~ electron escape length
 exp(-λ t) with λ ~ 2 nm



5.2 X-ray Photoemission Electron Microscopy (X-PEEM)



- Full Field Imaging
- 20 50 nm Resolution
- Linear and circular polarization

Courtesy H.Ohldag



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5.2 X-ray Photoemission Electron Microscopy (X-PEEM)

Iron whisker



Excitation by circularlypolarized electrons (MXCD)



Sensitivity



Courtesy C.M. Schneider

5.2 X-ray Photoemission Electron Microscopy (X-PEEM) Depth-selectivity by element-specific PEEM imaging



Fe-Cr-Co layer system



XMCD detects the difference in absorption for the projection of the sample's magnetization onto the propagation direction of circularly polarized X rays. XMCD distinguishes between magnetization parallel and antiparallel to the light **propagation** direction (in-plane magnetization at perpendicular incidence: no XMCD)



XMLD detects the difference in absorption of the axis of magnetization aligned parallel or perpendicular to the E-field of the X-rays.

XMLD distinguishes between the sample being magnetized parallel or perpendicular to the light **polarization** direction

5.2 X-ray Photoemission Electron Microscopy (X-PEEM) Layer-selective imaging

Tune to Co edge, use circular polarization: ferromagnetic domains



Interface studies of Ferromagnets on Antiferromagnets



Interface studies of Ferromagnets on Antiferromagnets



Chemically induced interfacial Ni spins provide the magnetic link



6.1 Scanning Electron Microscopy with Polarization Analysis



Mott detector:

Scattering of polarized electrons by gold foil is asymmetric (spin-orbit coupling effects)

(SEMPA)

- Secondary electrons are spin polarized, moment along magnetization direction
- Surface sensitive (secondary electrons emerge from top nanometer)
- Quantitative (independent measurement of 3 magnetization components)
- Resolution in 10 nm range

6.1 Scanning Electron Microscopy with Polarization Analysis

Basal plane of Co crystal



"Wheel side" of amorphous ribbon

courtesy J. Unguris



Polar components



In-plane components



Topography



In-plane components

6.2 Spin-polarized Tunneling Microscopy

- Tunneling of spin-polarized current between tip and sample surface
- Tunneling resistance depends on relative orientation of current polarity and domain magnetization
- Extreme resolution

M. Julliere, Phys. Lett. 54A, 225 (1975):







from Wiesendanger homepage

http://www.nanoscience.de/nanojoom/index.php/en/methods/sp-stm.html

6.2 Spin-polarized Tunneling Microscopy





Writing and Deleting Single Magnetic Skyrmions. Niklas Romming et al. Science 341, 636 (2013); DOI: 10.1126/science. 1240573

Fig. 1. Magnetic field dependence of the PdFe bilayer on the Ir(111) surface at T = 8 K. (A to C) Perspective sketches of the magnetic phases. (D) Overview SP-STM image, perspective view of constant-current image colorized with its derivative. (E to G) PdFe bilayer at different magnetic fields (U = +50 mV, I = 0.2 nA, magnetically out-of-plane sensitive tip). (E) Coexistence of spin spiral and skyrmion phase. (F) Pure skyrmion phase. (G) Ferromagnetic phase. A remaining skyrmion is marked by the white circle.

Sensitivity of imaging methods

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- Sensitive to H_{stray}

Sensitive to M

- \cdot Sensitive to ${m B}$
- Sensitive to distortions

- 1. Bitter technique
- 2. Magnetic force microscopy
- 3. Hall probe microscopy
- 4. Magneto-optical microscopy
- 5. X-ray spectroscopy
- 6. Polarized electrons (SEMPA, SPT)
- Transmission electron microscopy
- X-ray, neutron scattering



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Principle

- Electrons are deflected by Lorentz force
 - $F_{L} = q_{e} (v_{e} \times B)$ $q_{e}: \text{ Electron charge}$ $v_{e}: \text{ Electron velocity}$ B: Magnetic flux density
- Stray fields outside the sample contribute to contrast



Net deflection of electrons

Deflection by magnetization is canceled by deflections due to stray field No deflection by magnetization, stray field deflection cancels

- Tilting of sample may be required
- Maximum sample thickness: some 100 nm

7.1 Fresnel technique (defocused mode imaging)





- Out-of-focus: shadow effects delineate domain boundaries
- Magnetization direction can be derived from ripple (if present)



7.1 Fresnel technique (defocused mode imaging)

Fresnel imaging of differently sized magnetic particles (Co, 35 nm thick)





Courtesy J. Zweck

7.2 Foucault technique (in-focus)





Metallic glass, partially crystallized (courtesy J. Chapman)

7.3 Differential Phase Contrast (DPC) Microscopy



- Domain contrast like in Kerr microscopy
- Resolution better than 10 nm
- Quantitative determination of magnetization direction (by combining signals of a quadrant detector)

7.3 Differential Phase Contrast (DPC) Microscopy

In a scanning TEM



Permalloy, 60 nm thick (courtesy J. Chapman)

In a conventional TEM



AFM coupled Co-Cr-Co sandwich (courtesy J.P. Jakubovics)

Difference between Foucault images, obtained at different angles of incidence



- Magnetization influences phase of electron wave
- Phase gradient is perpendicular to B_0
- Lines of constant phase are parallel to B_0
- Flux between two lines is equal to flux quantum h/q_e

Electron Holography:

- Interference pattern of 2 electron waves shifted in phase
- Evaluation in optical interferometer

7.4 Electron Holography



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- Lines of constant phase are parallel to B_0
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- Interference pattern of 2 electron waves shifted in phase
- Evaluation in optical interferometer

7.4 Electron Holography

Off-axis holography (Tonomura et al. 1980)



7.4 Electron Holography

Differential Holography (Mankos et al. 1994)

- Both interfering beams pass through sample along slightly different paths (distance: 10 nm)
- Reconstruction contains information about their phase difference
 - \rightarrow phase gradient is recorded, which is proportional to magnetization
 - \rightarrow "real" domain images like in Kerr microscopy
- Quantitative information about magnetization direction at high resolution



Co/Au/Ni/Al multilayer (courtesy M. McCartney)



30 nm Co film (courtesy M. Scheinfein)

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8. X-ray, neutron scattering

8.1 X-ray Topography

- Plane-parallel X-ray beam, restricted to narrow strip
- Bragg condition fulfilled for some set of lattice planes
- Diffracted beam recorded by photographic plate
- Crystal and plate are advanced synchronously (scanning)

Contrast mechanism:

- Magnetostrictive strains disturb Bragg reflection
- Contrast at those positions, where rotation or spacing of lattice changes





Change of lattice orientation at 90° wall (10 - 5 radian)

8.1 X-ray Topography

X-ray topogram of fir-tree domains on slightly misoriented (100) FeSi crystal (0.1 mm thick)





(Courtesy J. Miltat)



C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)

Imaae detektor







C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)











C. Grünzweig, et al., Phys. Rev. Lett. 101, 025504 (2008)

















Principle:

Unpolarized neutrons, refracted at domain walls, locally destroy the interference pattern



Bright contrast is caused by refraction
Dark field imaging



Bright contrast is caused by refraction
Dark field imaging



→ Magnetic field



Steel plate, 2 mm thick









→ Magnetic field



Steel plate, 2 mm thick

Phase Theory and M(H) curve

Infinite or closed sample Finite sample $N = 0 \rightarrow H_{in} = H_{ext}$ $N \neq 0 \rightarrow H_{\text{ext}} = H_{\text{in}} + N \cdot \overline{M} \rightarrow \text{shearing}$ Rotation $M/M_{\rm s}$ $M/M_{\rm s}$ "knee" 0.9 0.9 "knee" **H**_{ext} 0.8 0.8 > $1/\sqrt{2}$ $1/\sqrt{2}$ \overrightarrow{H}_{ext} $H_{\rm ext}$ Mode III 0.6 0.6 0.5 0.5 $H_{\rm in} = 0$ Wall displacement 0.4 $H_{\rm in} = 0$ 0.3 0.3 $H_{\rm ext}$ Mode I 0.2 0.2 0.1 0.1 0 0 0.2 $\mathbf{0}$ 0.4 0.6 0.8 0.2 0.4 0.6 0.8 0 $H_{\rm ext}/H_{\rm K} = H_{\rm in}/H_{\rm K}$ $H_{\rm ext}/H_{\rm K}$



→ Magnetic field



Steel plate, 2 mm thick









Non-oriented FeSi steel

Together with B. Betz and C. Grünzweig (PSI Villigen), R. Siebert (Fraunhofer IWS Dresden) unpublished







I. Manke, et al.: Three-dimensional imaging of magnetic domains. Nature Communications, 1:125 doi: 10.1038/ncomms1125 (2010)

Comparison of Domain Obervation Techniques



MFM: Magnetic Force Microscopy SPT: Spin-Polarized Tunneling SEM: Scanning (reflection) Electron Microscopy TEM: Transmission Electron Microscopy