

Fundamentals of Magnetism

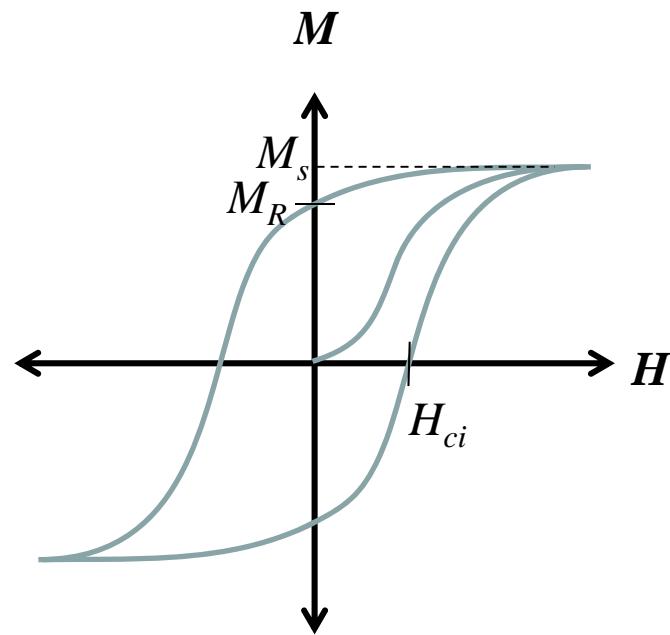
Part II

Albrecht Jander

Oregon State University

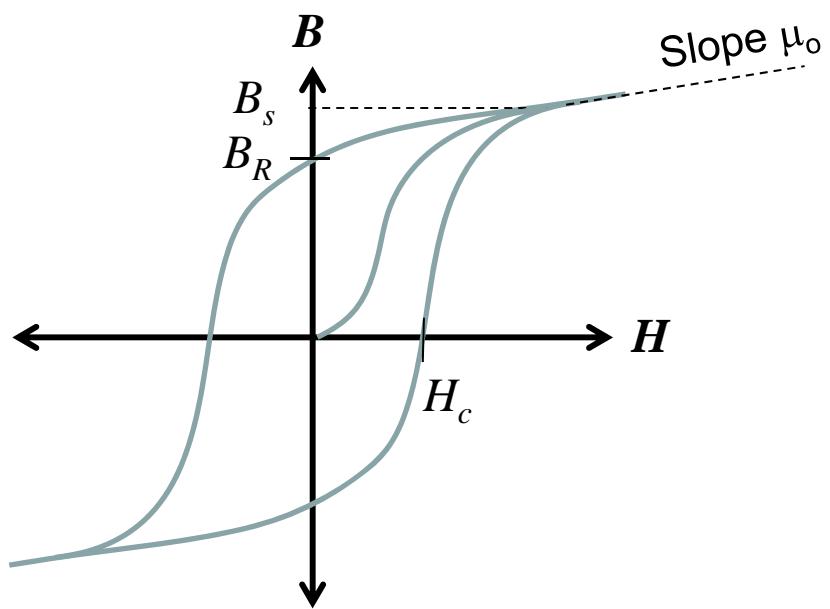
Real Magnetic Materials, Bulk Properties

M-H Loop



M_s - Saturation magnetization
 H_{ci} - Intrinsic coercivity
 M_R - Remanent magnetization

B-H Loop

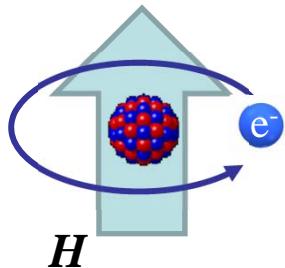


B_s - Saturation flux density
 B_R - Remanent flux density
 H_c - Coercive field, coercivity

Note: these two figures each present the same information because $B = \mu_0(H + M)$

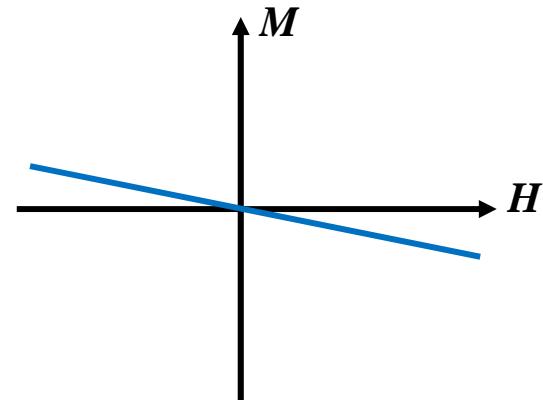
Diamagnetism

- Atoms without net magnetic moment



Diamagnetic substances:

| | | |
|-----------------------|-----------------|-----------------------|
| Ag | | -1.0x10 ⁻⁶ |
| Be | | -1.8x10 ⁻⁶ |
| Au | | -2.7x10 ⁻⁶ |
| H ₂ O* | | -8.8x10 ⁻⁶ |
| NaCl | | -14x10 ⁻⁶ |
| Bi | | -170x10 ⁻⁶ |
| Graphite | | -160x10 ⁻⁶ |
| Pyrolytic graphite | (\perp) | -450x10 ⁻⁶ |
| | (\parallel) | -85x10 ⁻⁶ |



χ is small and negative

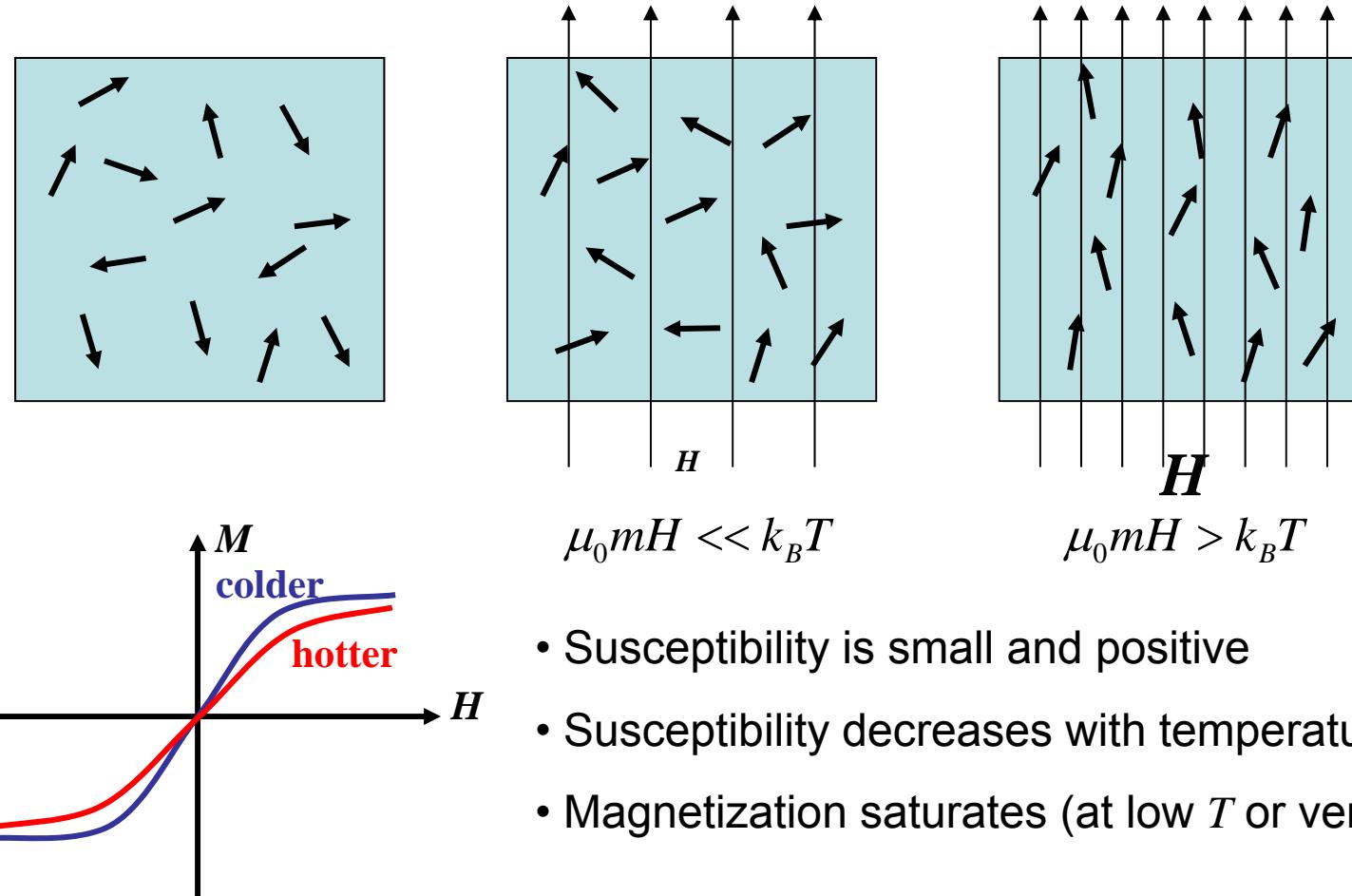
$$\chi = -\frac{N_A \rho}{W_A} \frac{\mu_0 Z e^2 r^2}{6 m_e}$$

Atomic number
Atomic density
Orbital radius

* E.g. humans, frogs, strawberries, etc.
See: <http://www.hfml.ru.nl/froglev.html>

Paramagnetism

- Consider a collection of atoms with independent magnetic moments.
- Two competing forces: spins try to align to magnetic field but are randomized by thermal motion.



Langevin Theory of Paramagnetism*

- Energy of a magnetic moment, m , in a field, H

$$E = -\mu_0 \vec{m} \cdot \vec{H} = -\mu_0 m H \cos(\theta)$$

- Independent moments follow Boltzmann statistics

$$P(E) = e^{-E/k_B T} = e^{\mu_0 m H \cos(\theta)/k_B T}$$

- The “density of states” on the sphere is

$$dn = 2\pi r^2 \sin(\theta) d\theta$$

- So the probability of a moment pointing in direction θ to $\theta+d\theta$ is

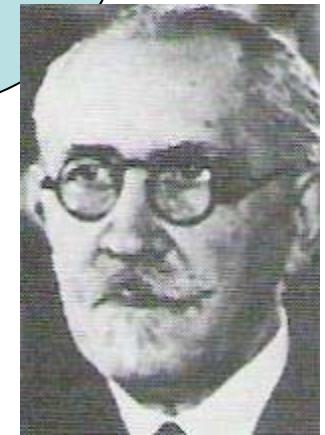
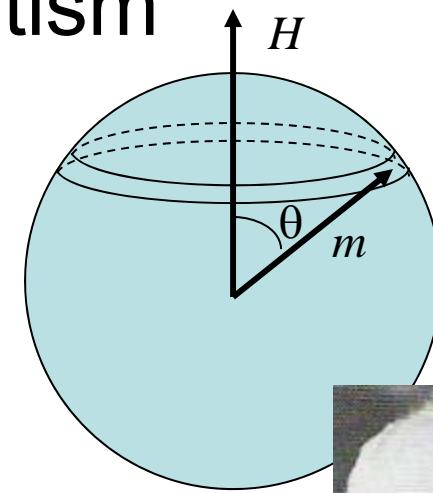
$$p(\theta) = \frac{e^{\mu_0 m H \cos(\theta)/k_B T} \sin(\theta)}{\int_0^\pi e^{\mu_0 m H \cos(\theta)/k_B T} \sin(\theta) d\theta}$$

- The magnetization of a sample with N moments/volume will be

$$M = Nm \langle \cos(\theta) \rangle = Nm \int_0^\pi \cos(\theta) p(\theta) d\theta = Nm \frac{\int_0^\pi e^{\mu_0 m H \cos(\theta)/k_B T} \cos(\theta) \sin(\theta) d\theta}{\int_0^\pi e^{\mu_0 m H \cos(\theta)/k_B T} \sin(\theta) d\theta}$$

- Which any fool can see is just:

$$M = Nm \left[\coth \left(\frac{\mu_0 m H}{k_B T} \right) - \frac{k_B T}{\mu_0 m H} \right]$$



Paul Langevin
(1872-1946)

*Langevin, P., Annales de Chem. et Phys., 5, 70, (1905).

Curie's Law*

- Langevin paramagnetism:

$$M = Nm \left[\coth\left(\frac{\mu_0 m H}{k_B T}\right) - \frac{k_B T}{\mu_0 m H} \right]$$

- For $\mu_0 m H \ll k_B T$ (most practical situations)

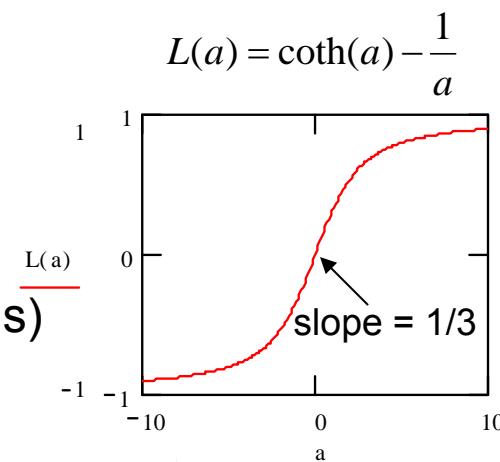
$$M = \mu_0 \frac{Nm^2}{3k_B T} H$$

- Which gives Curie's Law:

$$\chi = \frac{M}{H} = \mu_0 \frac{Nm^2}{3k_B T} = \frac{C}{T}$$

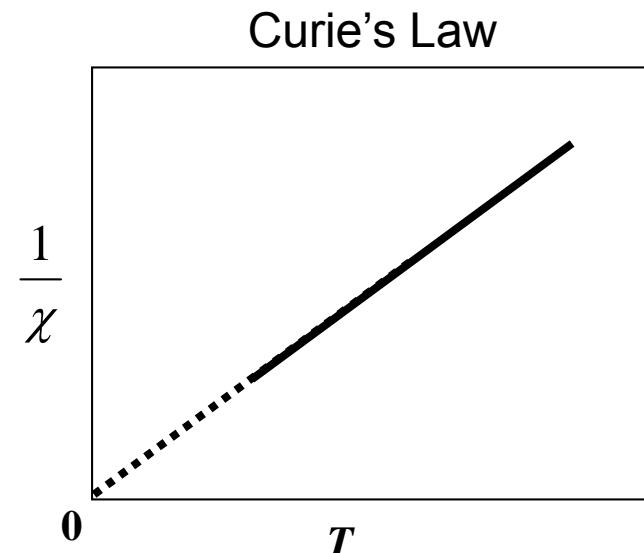
Note: quantization of the magnetic moment requires a correction to the above classical result which assumes all directions are allowed:

$$\chi = \frac{M}{H} = \mu_0 \frac{Ng^2 \mu_B^2 J(J+1)}{3J^2 k_B T} = \frac{C}{T}$$



Pierre Curie
(1859-1906)

Curie constant



*Curie, P., Ann. Chem. Phys., 5, 289 (1895)

Paramagnetic Substances

Paramagnetic susceptibility:

| | |
|----------------------|-----------------------|
| Sn | 0.19×10^{-6} |
| Al | 1.65×10^{-6} |
| O ₂ (gas) | 1.9×10^{-6} |
| W | 6.18×10^{-6} |
| Pt | 21.0×10^{-6} |
| Mn | 66.1×10^{-6} |

Liquid oxygen



Curie-Weiss* Law

- Consider interactions among magnetic moments:

$$E = -\mu_0 \vec{m} \cdot (\vec{H} + \alpha \vec{M})$$

where M represents the average orientation of the surrounding magnetic moments. (“Mean field theory”) and α is the strength of the interactions

- The Langevin equation then becomes:

$$M = Nm \left[\coth \left(\frac{\mu_0 m (H + \alpha M)}{k_B T} \right) - \frac{k_B T}{\mu_0 m (H + \alpha M)} \right]$$

- Again for $\mu_0 m H \ll k_B T$

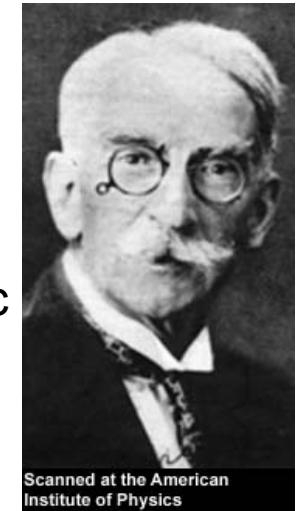
$$M = \mu_0 \frac{Nm^2}{3k_B T} (H + \alpha M)$$

- Which gives the Curie-Weiss Law:

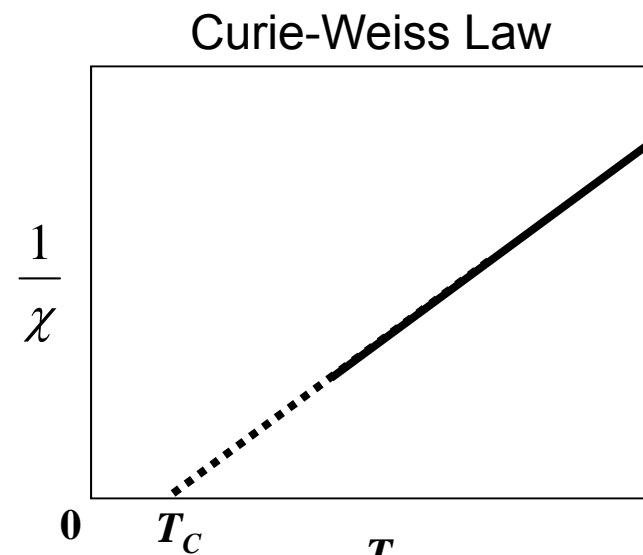
$$\chi = \frac{M}{H} = \frac{C}{T - \alpha C} = \frac{C}{T - T_c}$$

$$T_c = \mu_0 \frac{\alpha Nm^2}{3k_B}$$

Curie Temperature



Pierre Weiss
(1865–1940)



*Weiss, P., J. de Phys., **6**, 661 (1907)

Weiss Theory* of Ferromagnetism

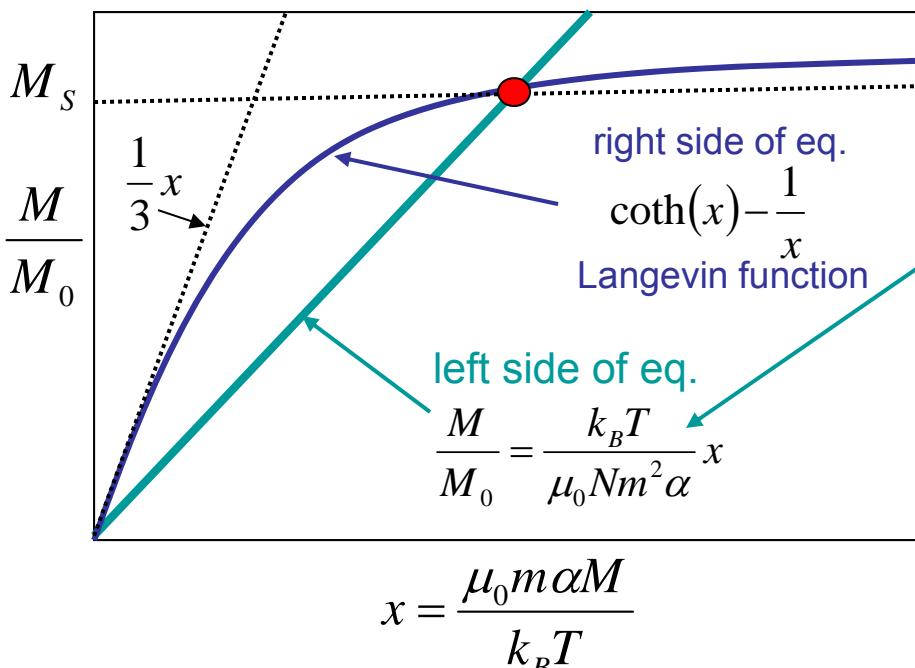
- Starting with the Langevin equation with “mean field” interactions

$$M = Nm \left[\coth\left(\frac{\mu_0 m(H + \alpha M)}{k_B T}\right) - \frac{k_B T}{\mu_0 m(H + \alpha M)} \right]$$

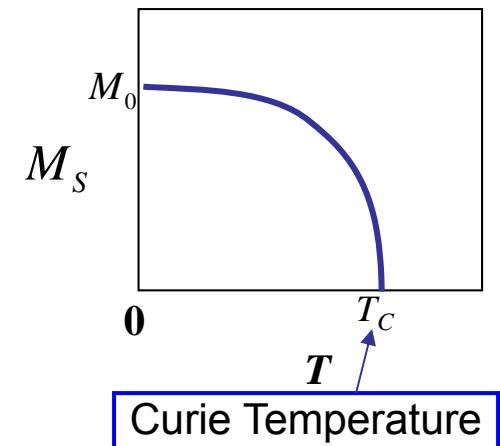
- Set the external field to zero, $H=0$

$$M = Nm \left[\coth\left(\frac{\mu_0 m(\alpha M)}{k_B T}\right) - \frac{k_B T}{\mu_0 m(\alpha M)} \right]$$

- This can be solved for M graphically:



*Weiss, P., J. de Phys., **6**, 661 (1907)



Plot both sides of the equation as a function of

$$x = \frac{\mu_0 m \alpha M}{k_B T}$$

Intersection is spontaneous magnetization, M_s

Note: line with slope proportional to T

Asymptote of Langevin function is $1/3$ so the only solution for M_s is zero when

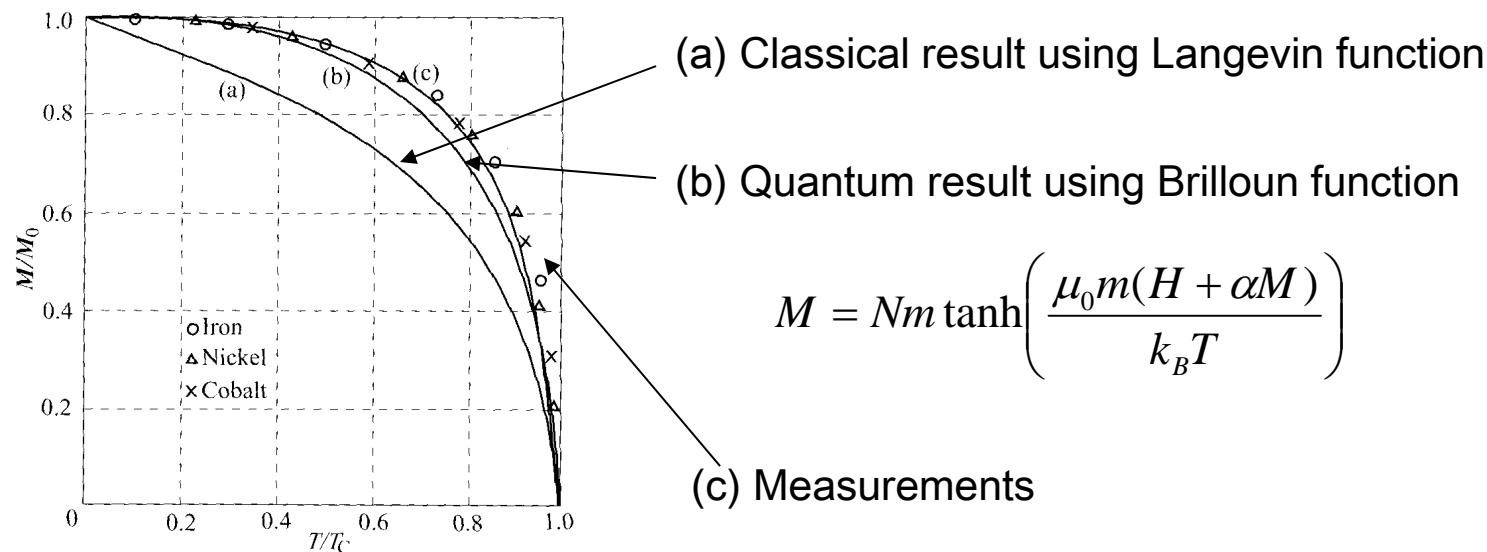
$$\frac{k_B T}{\mu_0 N m^2 \alpha} > \frac{1}{3}$$

Spontaneous magnetization decreases with temperature and vanishes at:

$$T_c = \frac{\mu_0 N m^2 \alpha}{3 k_B}$$

Weiss Theory of Ferromagnetism

- Fits data very well!
- Again, corrections need to be made for quantization of magnetic moments



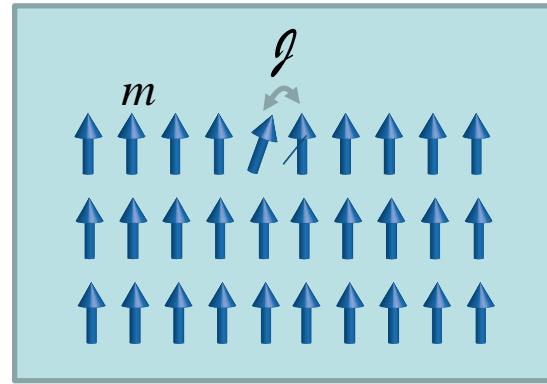
Points to remember:

- Ferromagnets have spontaneous magnetization, M_S even in zero field
- M_S goes to zero at the Curie temperature, T_C
- Above T_C material is paramagnetic.

Ferromagnetic Materials

| Material: | M_s [A/m] | T_c [$^{\circ}$ C] |
|-----------|------------------------|-----------------------|
| Ni | 0.49×10^6 | 354 |
| Fe | 1.7×10^6 | 770 |
| Co | 1.4×10^6 | 1115 |
| Gd | | 19 |
| Dy | | -185 |
| NdFeB | | 310 |
| NiFe | $\sim 0.8 \times 10^6$ | 447 |
| FeCoAlO | 1.9×10^6 | |

Ferromagnetic Exchange Interaction

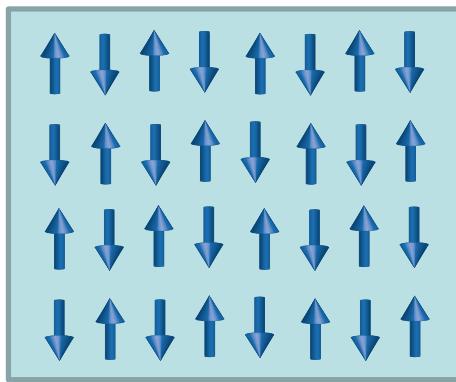


$$E_{m_i, m_{i+1}} = -\mu_0 J m^2 \cos(\Delta\theta)$$

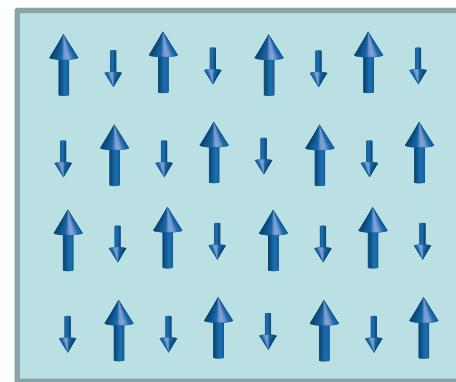
Antiferromagnetic and Ferrimagnetic Materials

Negative exchange coupling:

Antiferromagnet

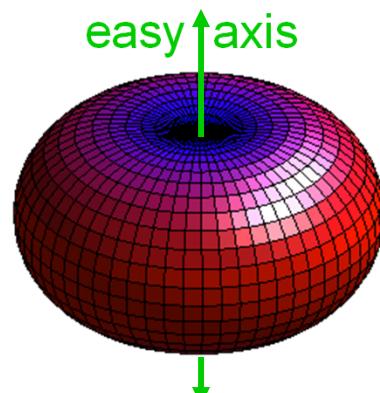


Ferrimagnet

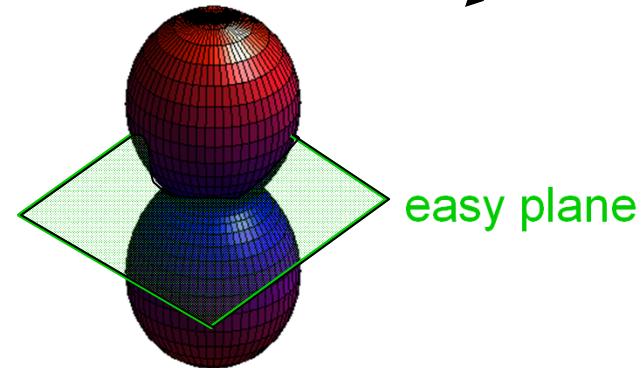


Crystalline Anisotropy

- Uniaxial: $E = K_u \sin^2 \theta + K_2 \sin^4 \theta + \dots$

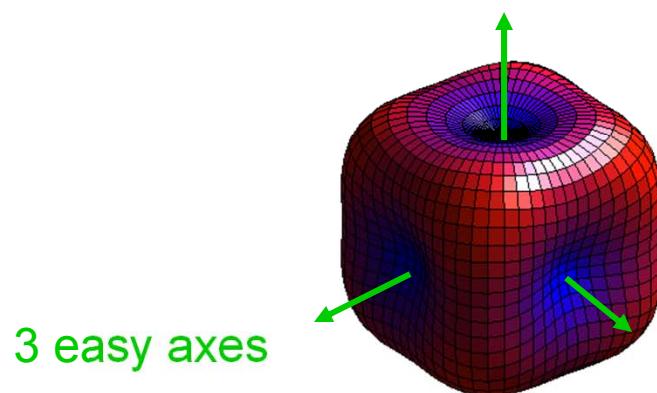


$$K_u > 0$$

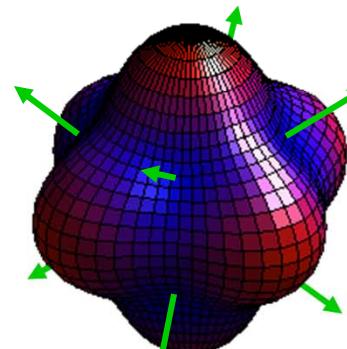


$$K_u < 0$$

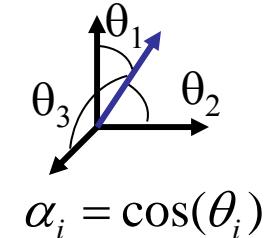
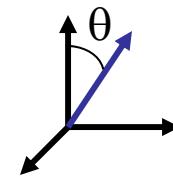
- Cubic: $E = K_1(\alpha_1^2 \alpha_2^2 + \alpha_2^2 \alpha_3^2 + \alpha_1^2 \alpha_3^2) + K_2(\alpha_1^2 \alpha_2^2 \alpha_3^2) + \dots$



$$K_1 > 0$$



$$K_1 < 0$$



$$\alpha_i = \cos(\theta_i)$$

4 easy axes

Crystalline Anisotropies of Some Magnetic Materials

| Material | Structure | A [J/m] x10 ⁻¹¹ | K ₁ [J/m ³] x10 ⁵ | K ₂ [J/m ³] x10 ⁵ |
|-------------------|-----------|-------------------------------|--|--|
| Cobalt | hcp | 1.5 | 4.1 | 1.5 |
| | | | | |
| Iron | bcc | 1.5 | 0.48 | -0.1 |
| Nickel | fcc | 1.5 | -0.045 | -0.023 |
| SmCo ₅ | | 2.4 | 170 | |

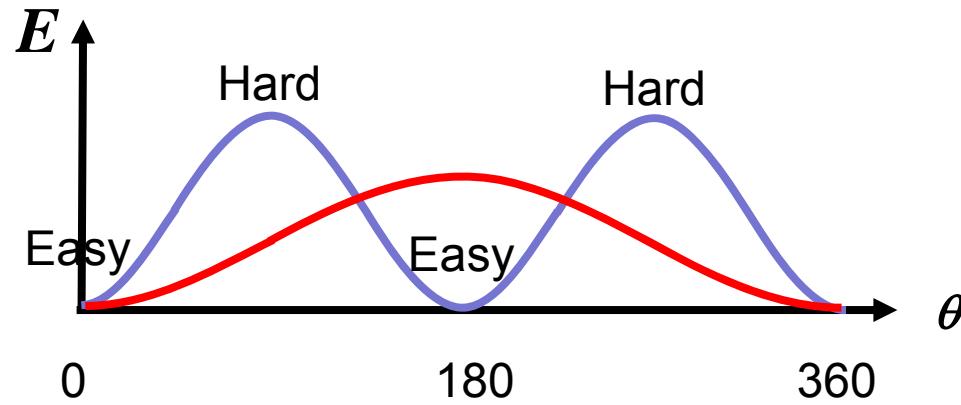
Stoner-Wohlfarth Theory*

Anisotropy energy

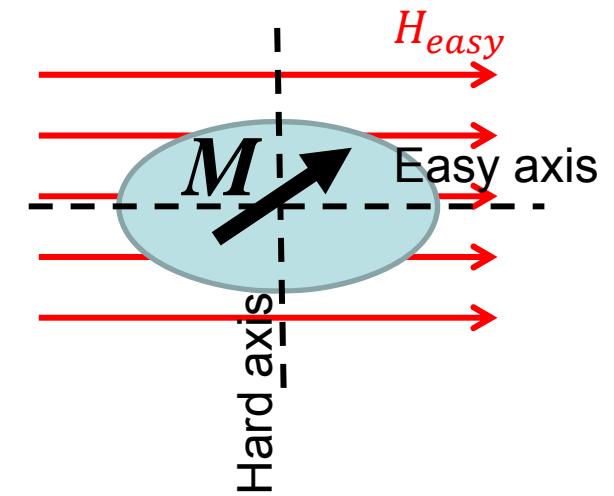
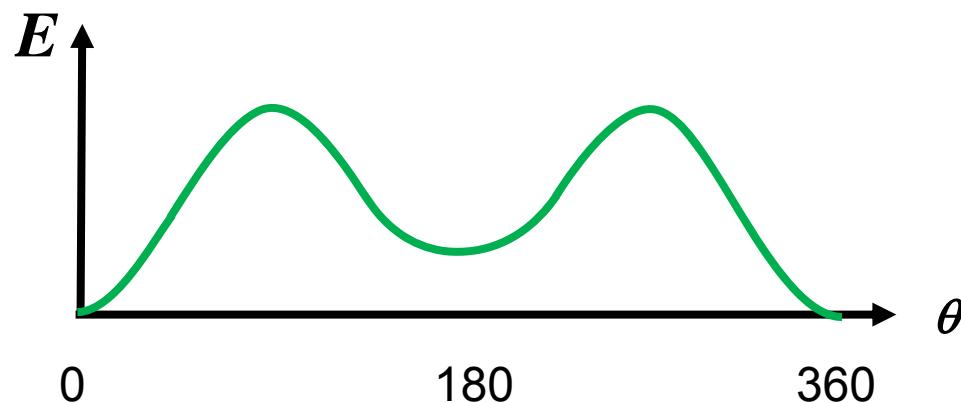
$$E_{anis} = K_u V \sin^2(\theta)$$

Magnetostatic energy

$$E_{ms} = H_{easy} M_s V \cos(\theta)$$



Total energy (Magnetic field along easy axis)



* E. Stoner and P. Wohlfarth, "A Mechanism of Magnetic Hysteresis in Heterogeneous Alloys", IEEE Trans. Magn., **27**, 3475, 1991

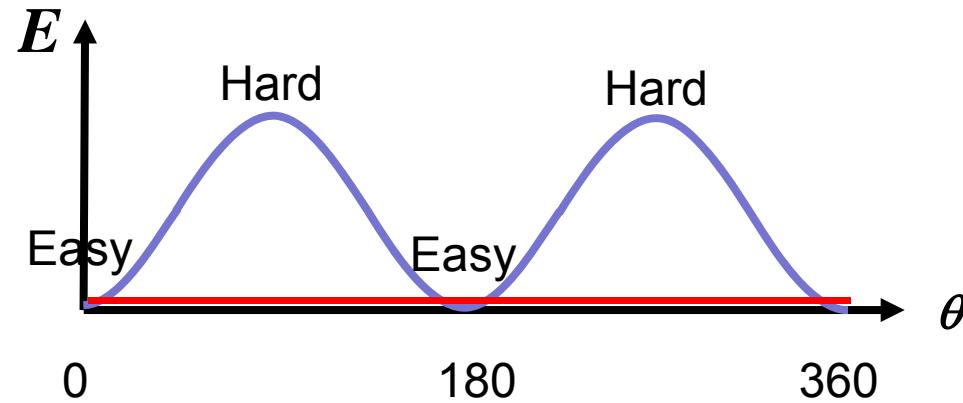
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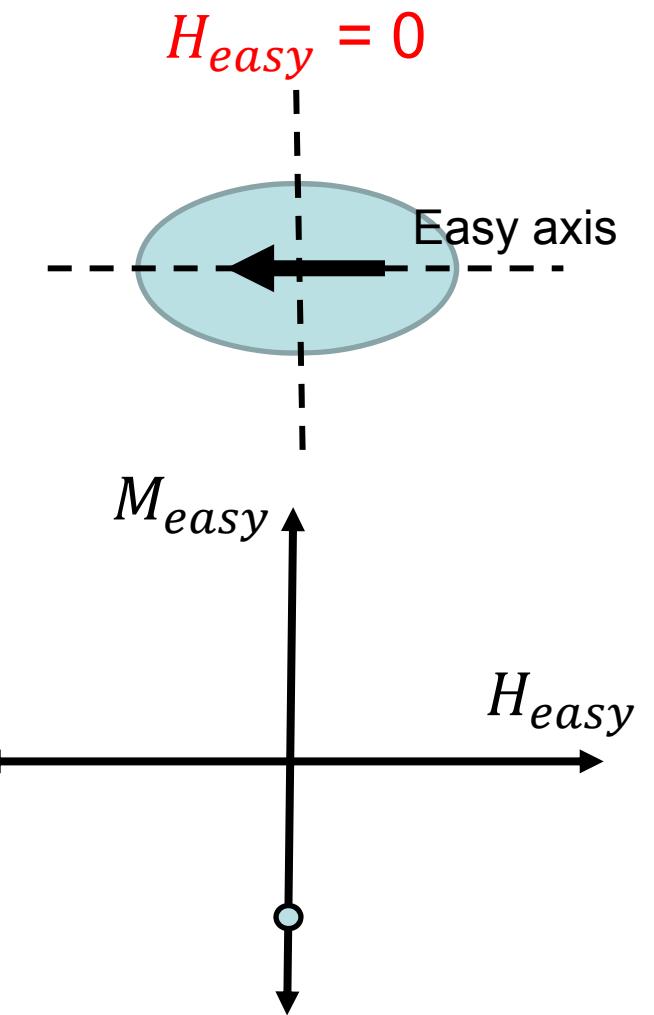
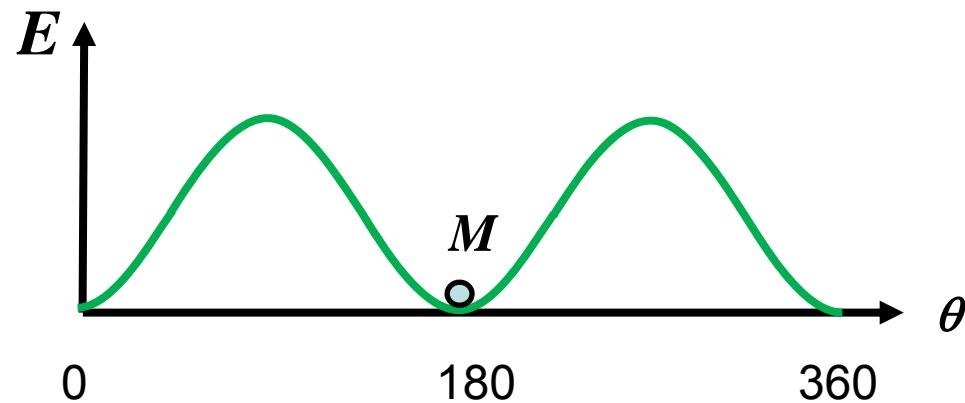
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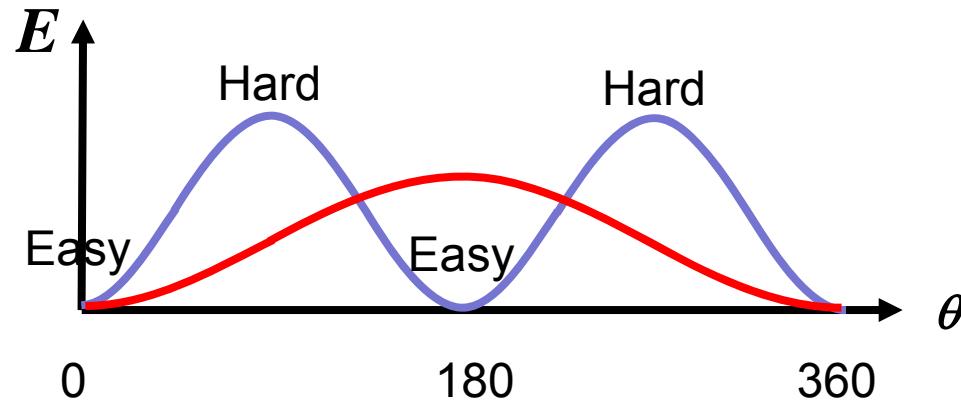
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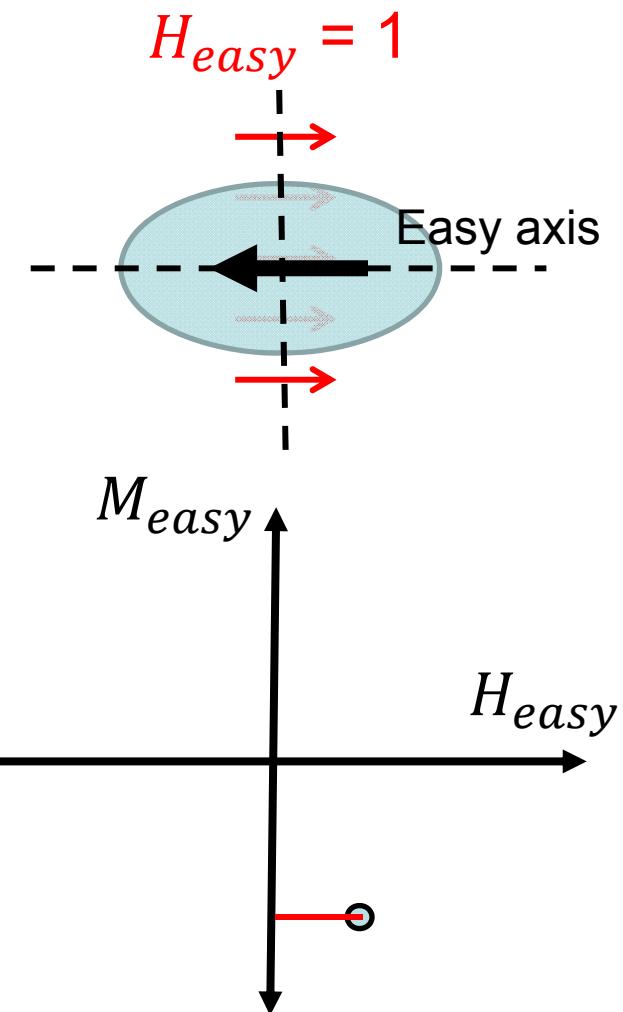
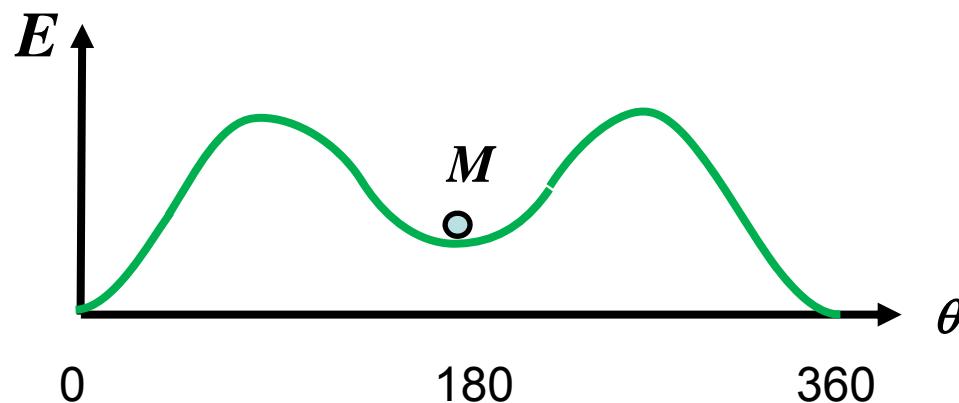
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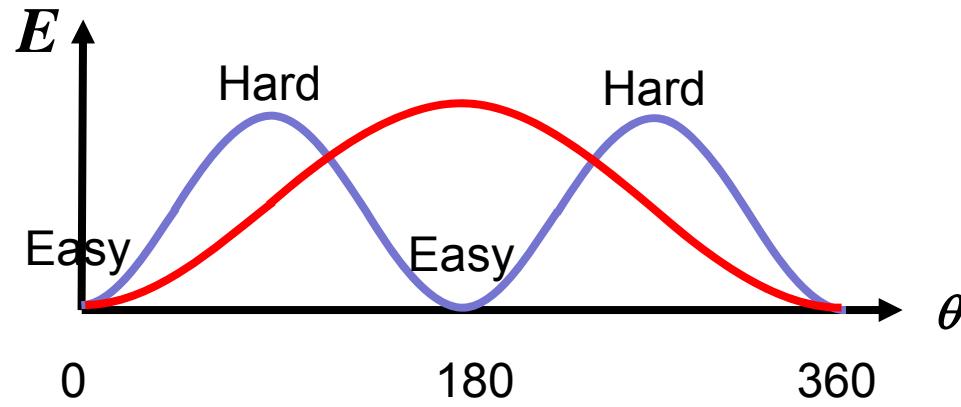
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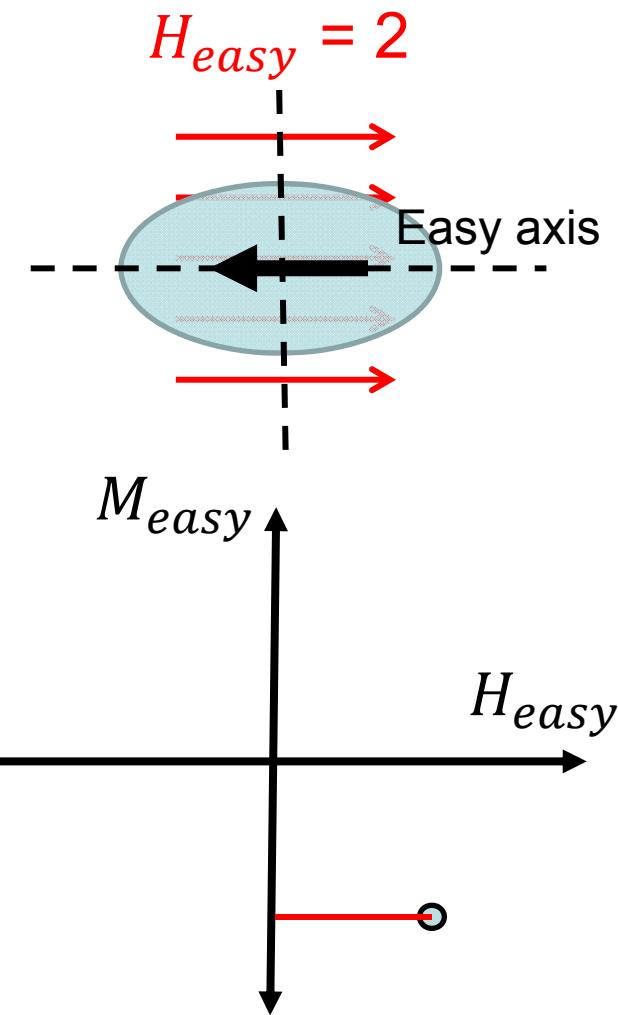
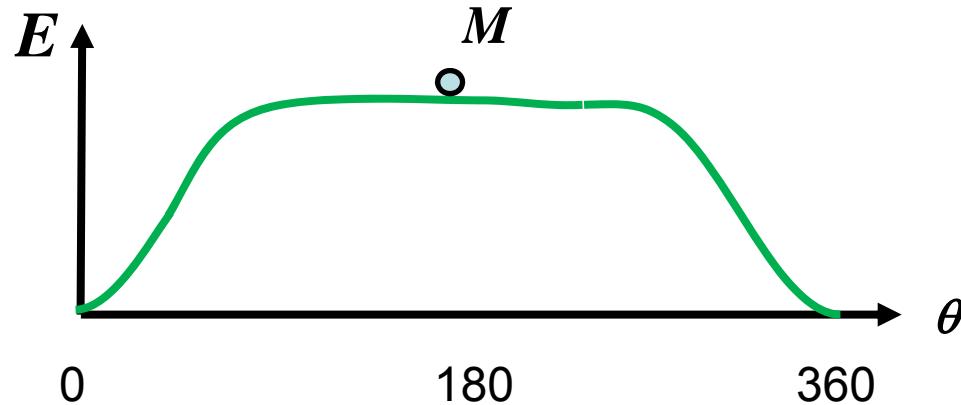
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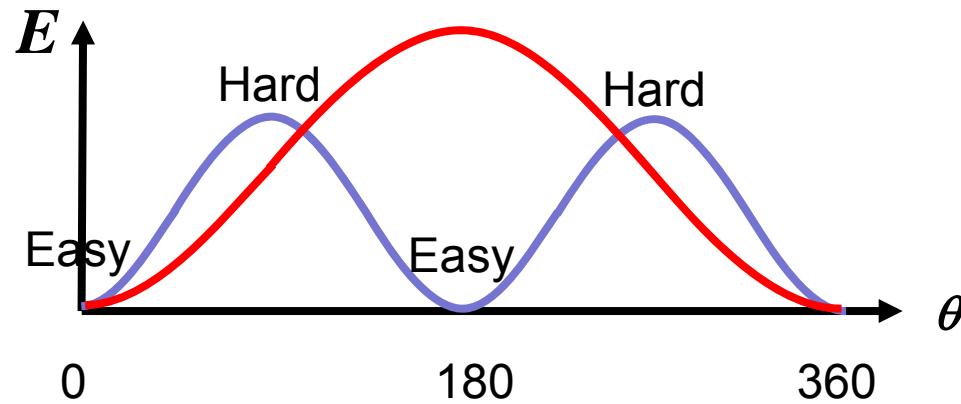
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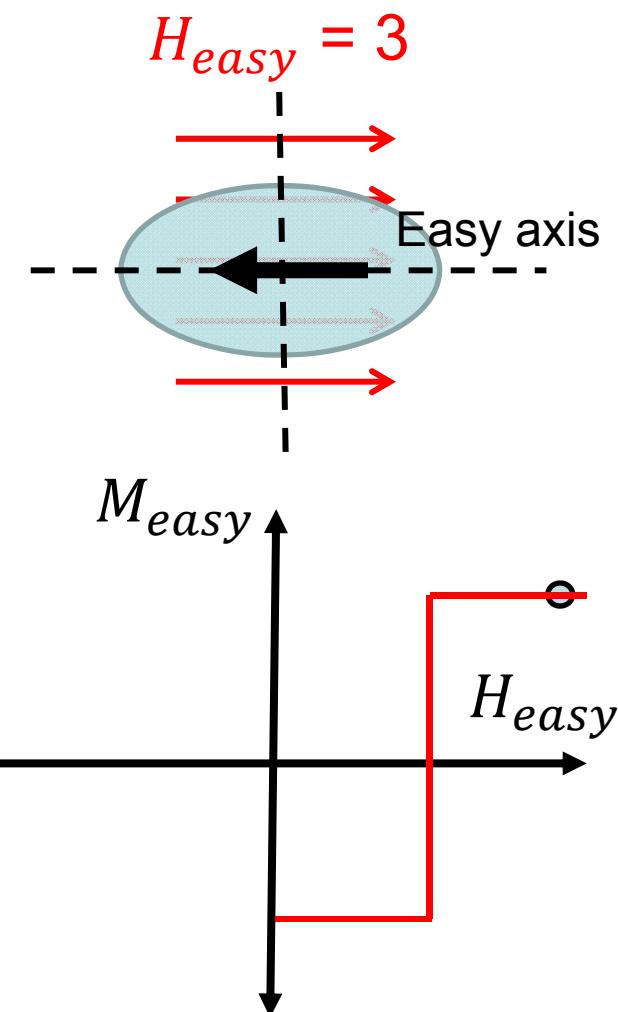
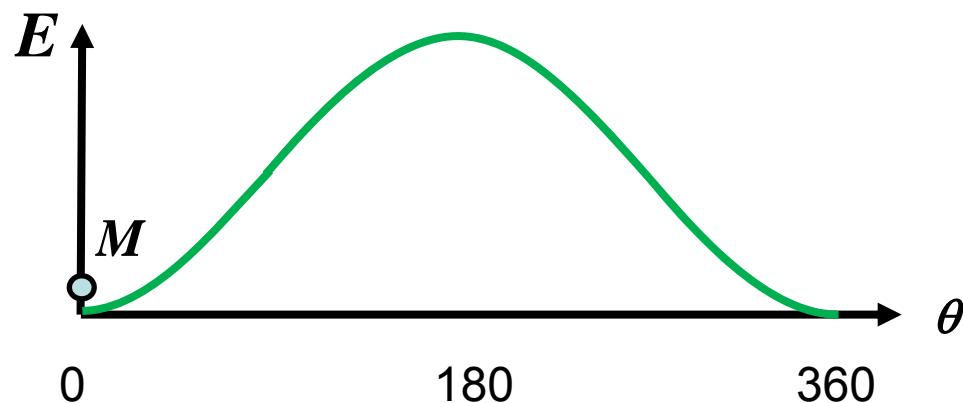
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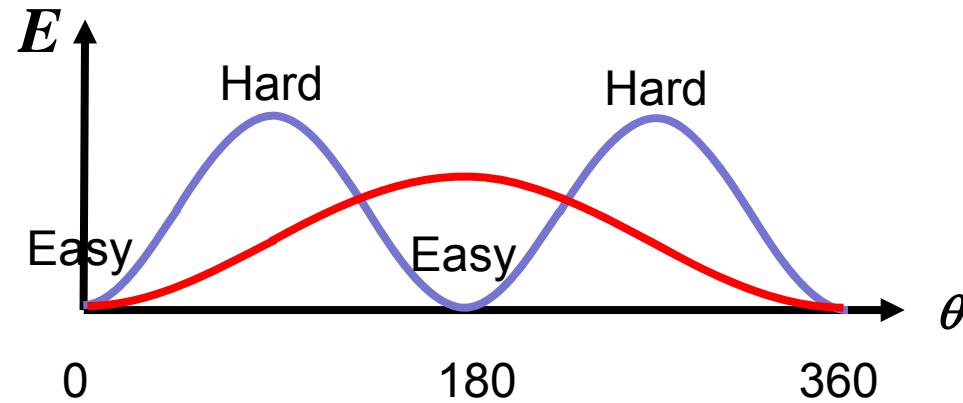
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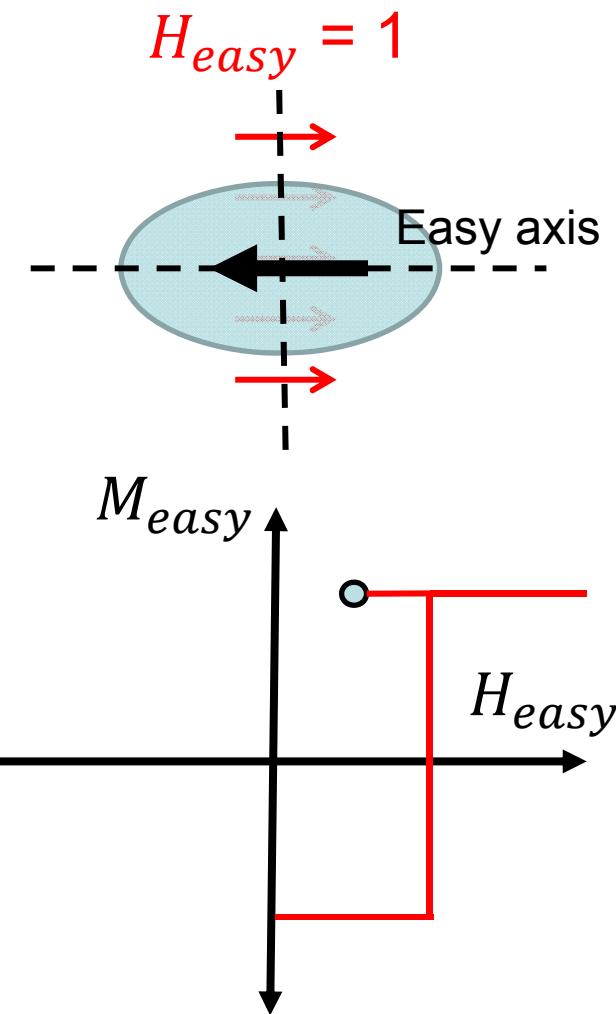
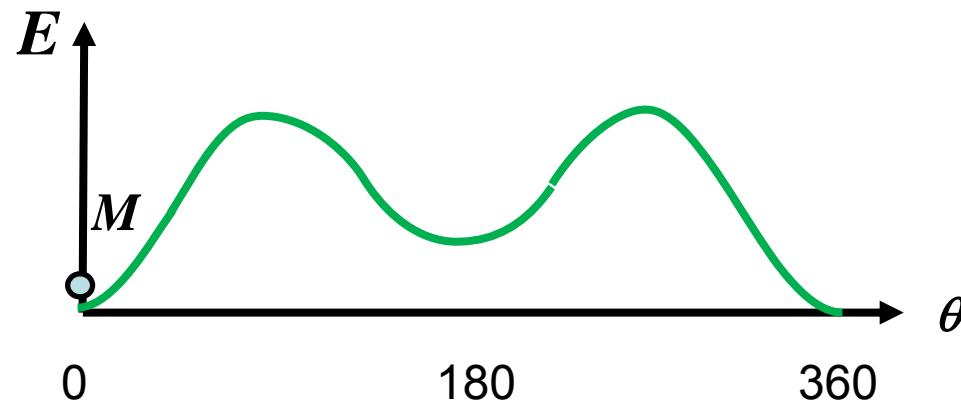
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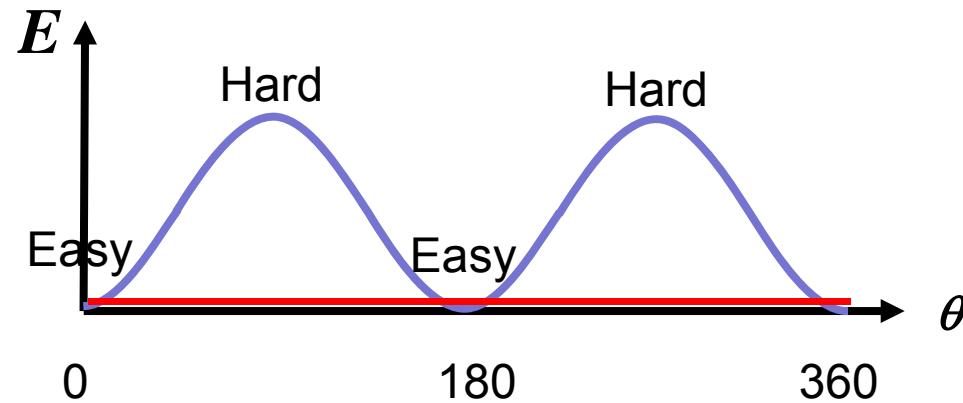
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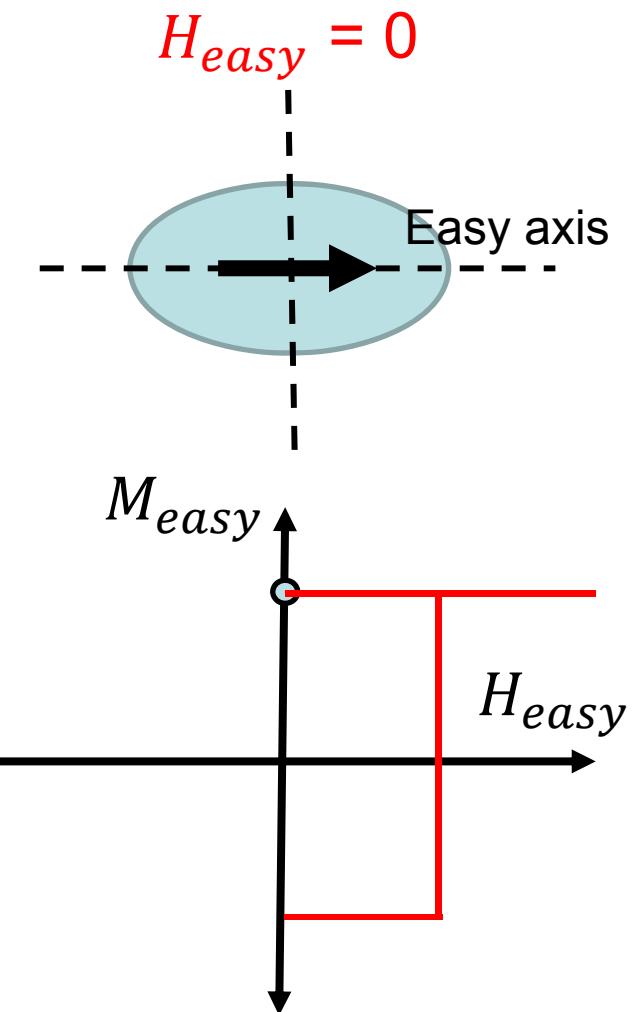
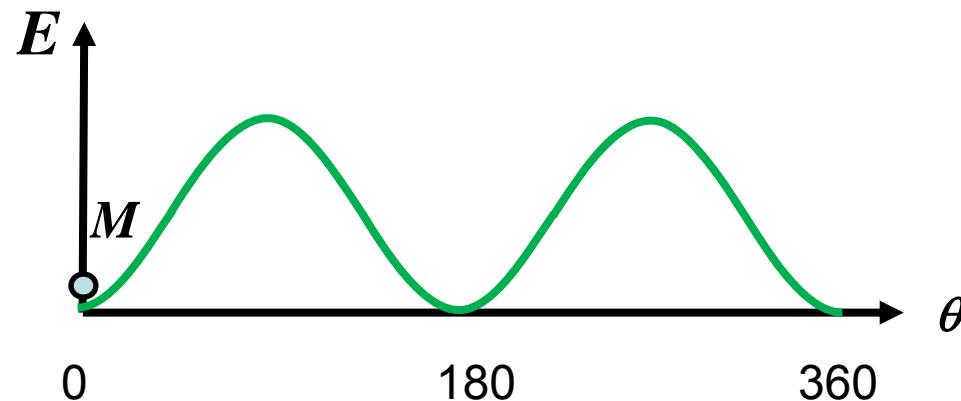
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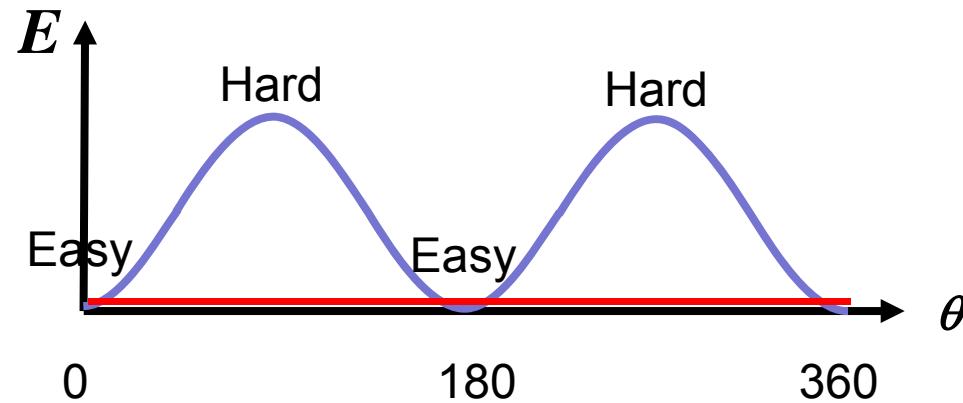
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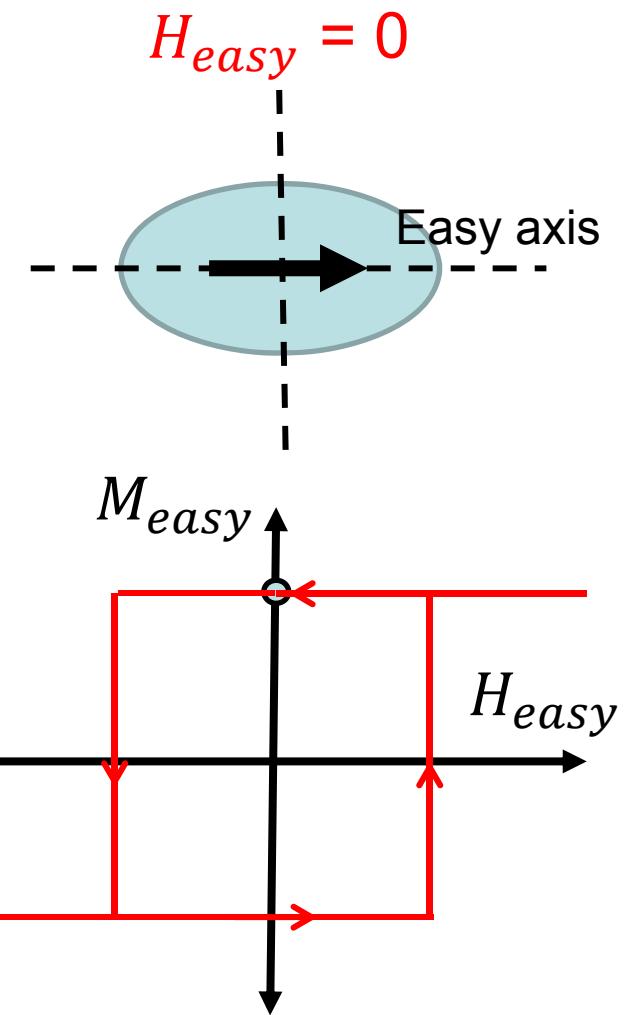
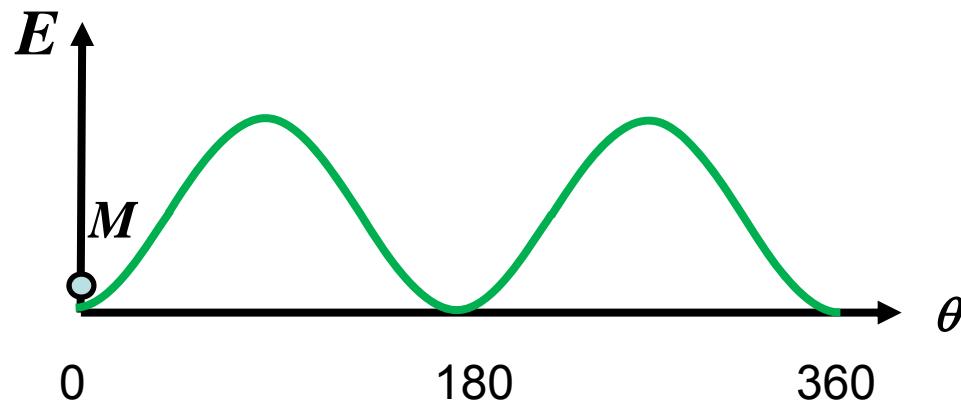
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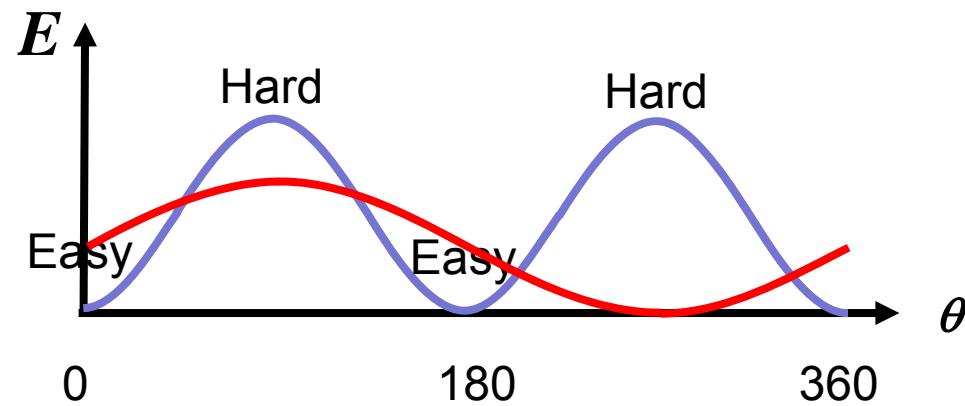
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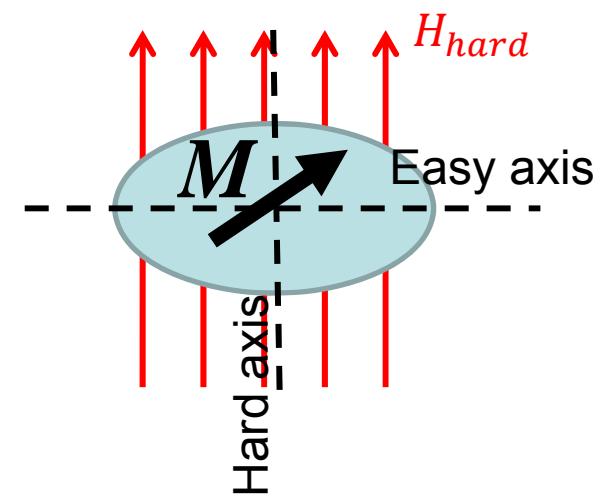
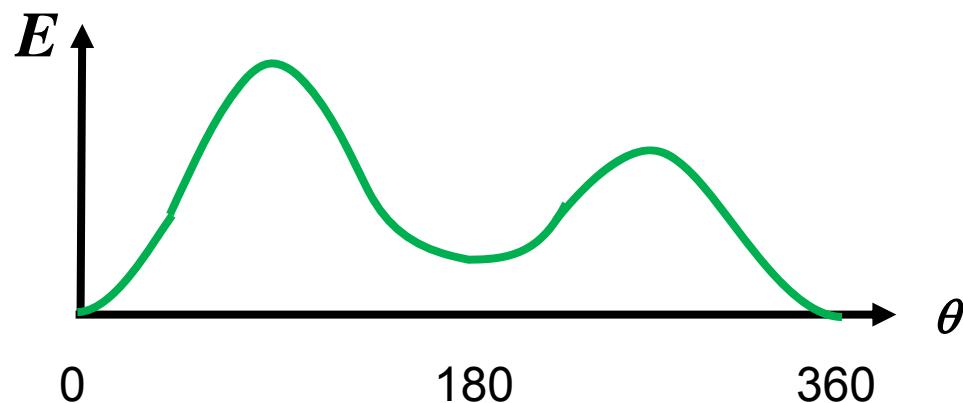
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Total energy (Magnetic field along easy axis)



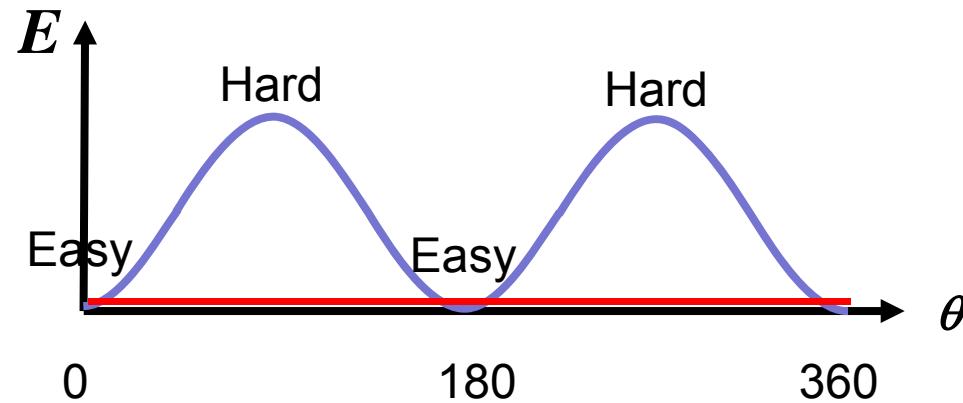
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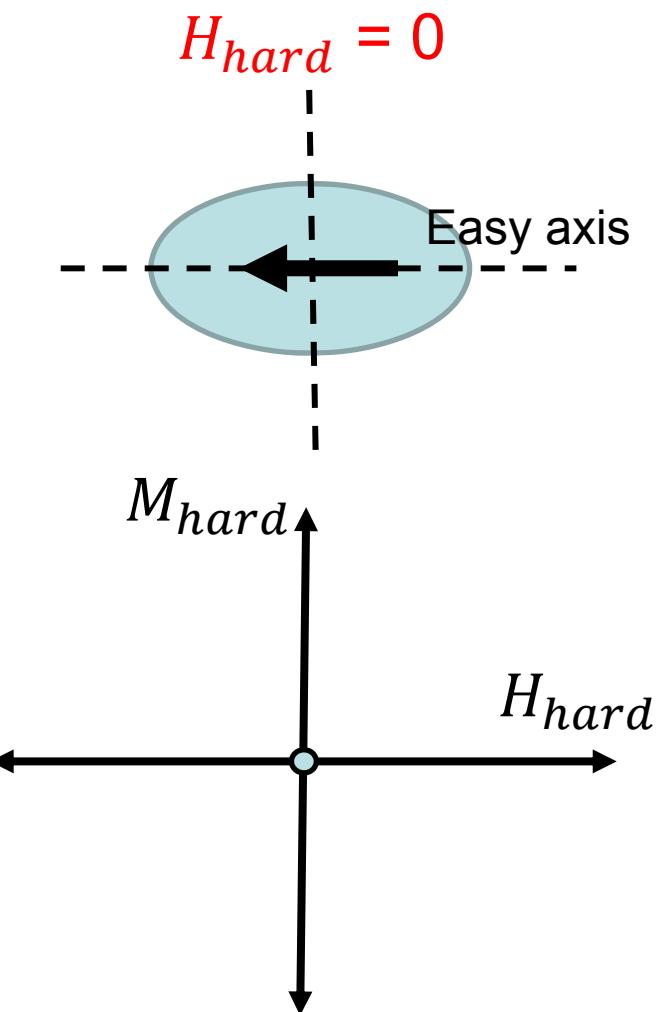
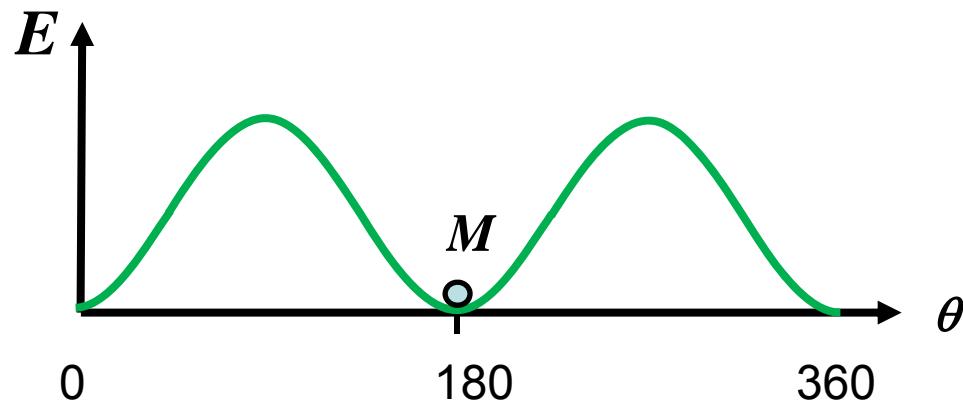
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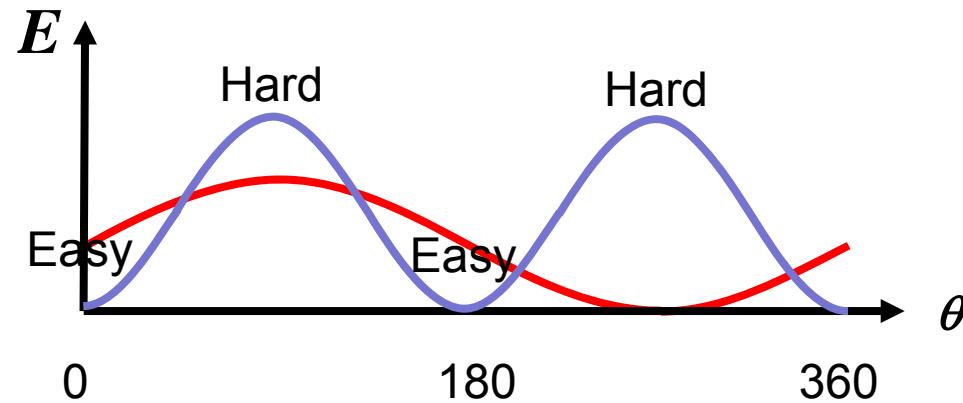
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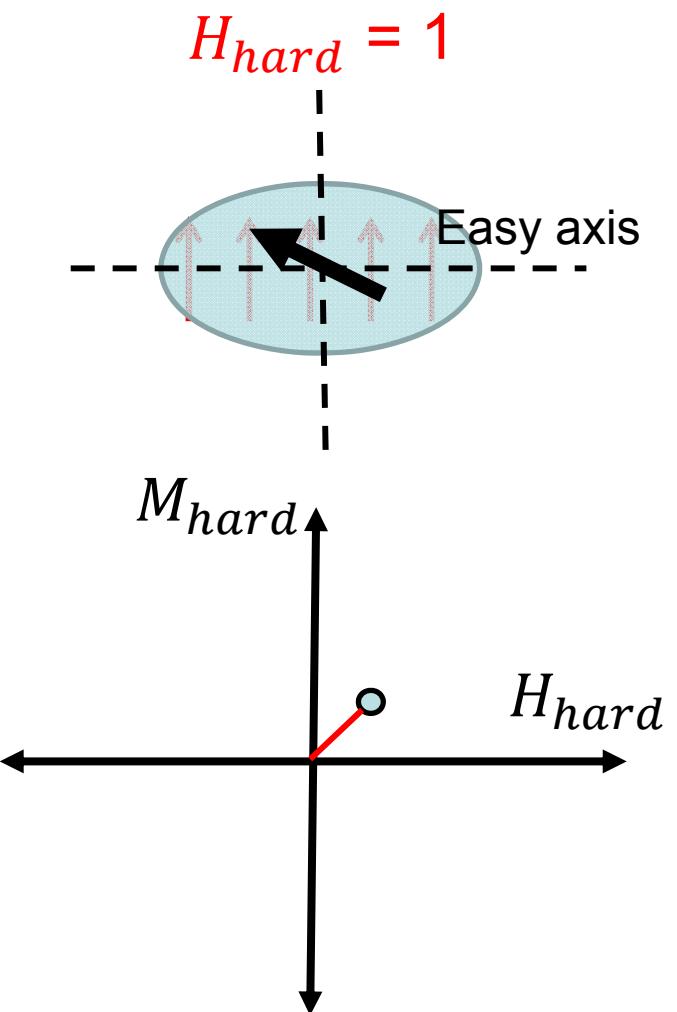
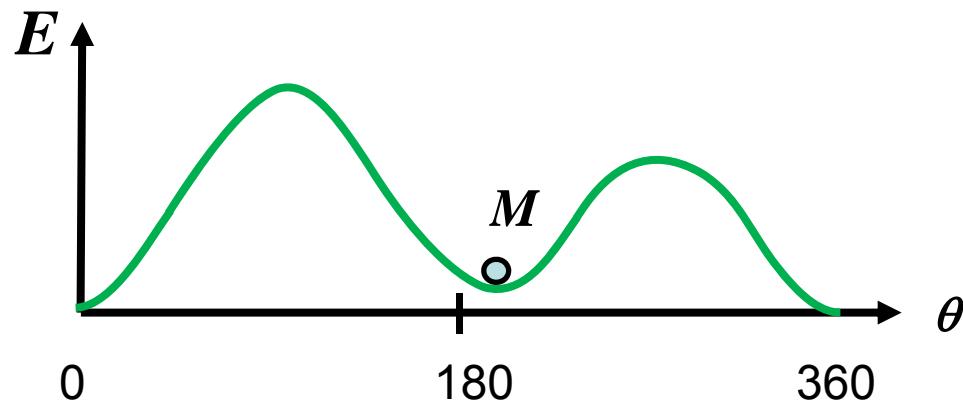
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$$E_{ms} = H_{hard} M_s V \sin(\theta)$$



Total energy (Magnetic field along easy axis)



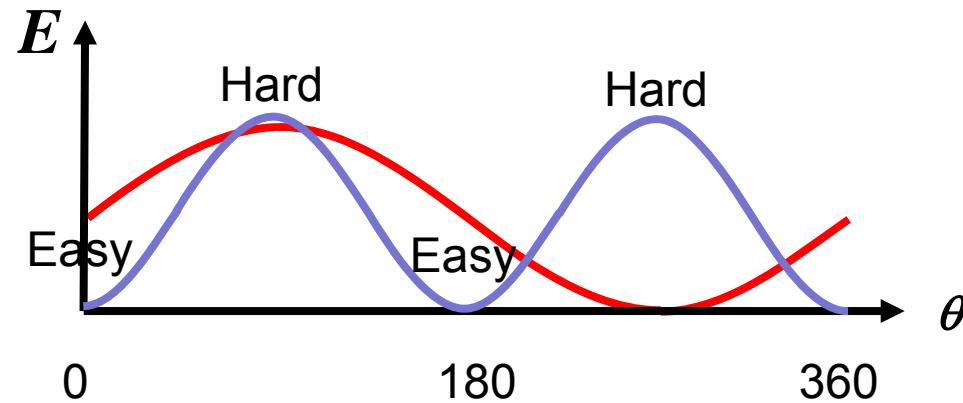
Stoner-Wohlfarth Theory*

Anisotropy energy

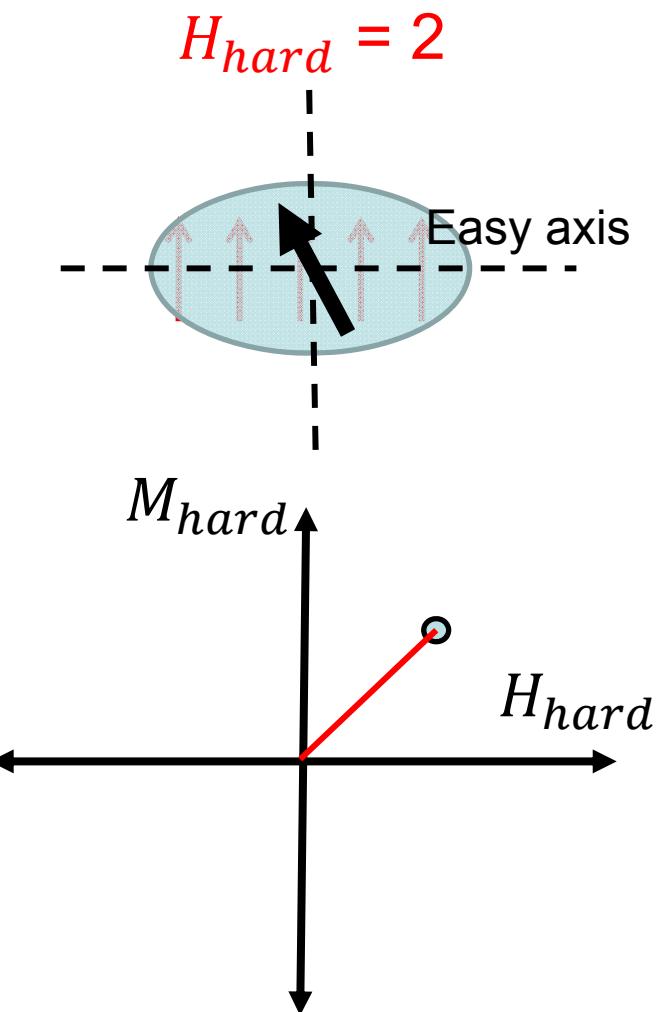
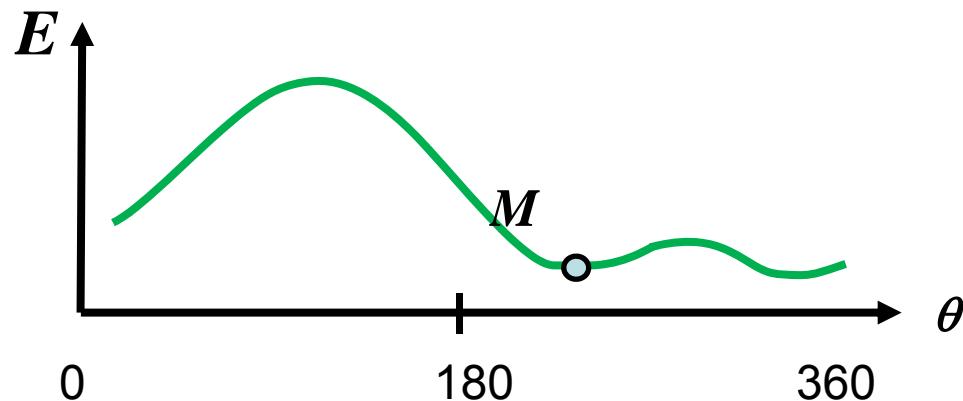
$$E_{anis} = K_u V \sin^2(\theta)$$

Magnetostatic energy

$$E_{ms} = H_{hard} M_s V \sin(\theta)$$



Total energy (Magnetic field along easy axis)



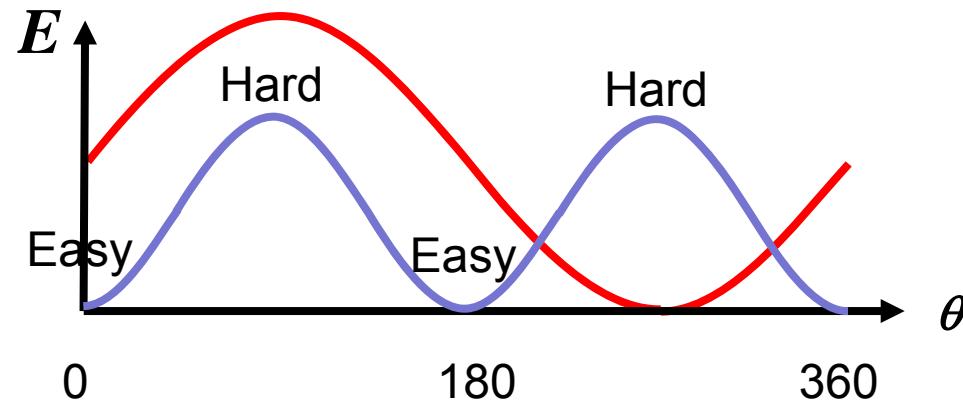
Stoner-Wohlfarth Theory*

Anisotropy energy

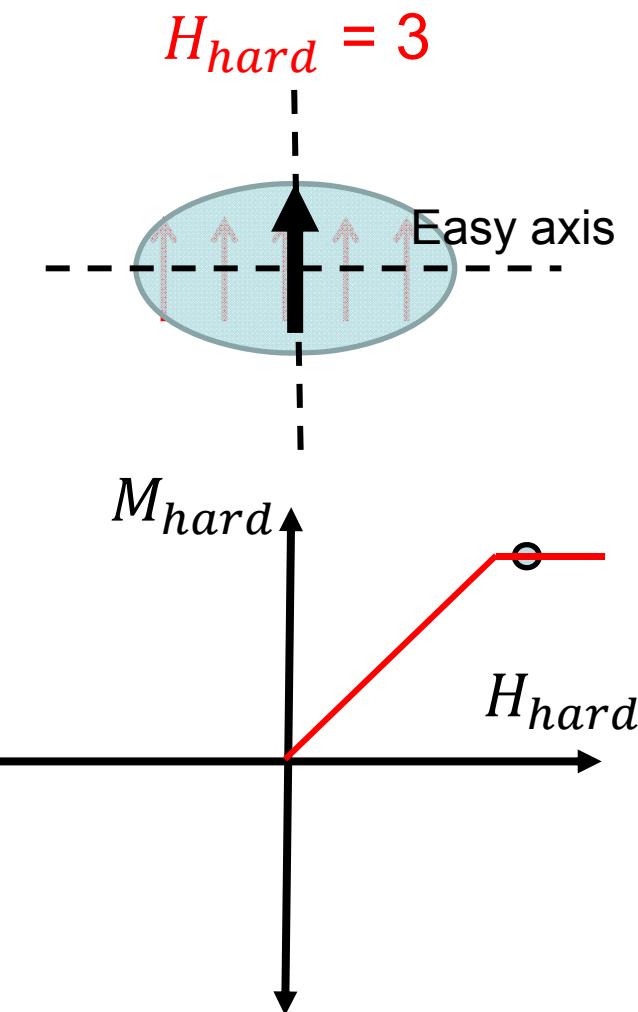
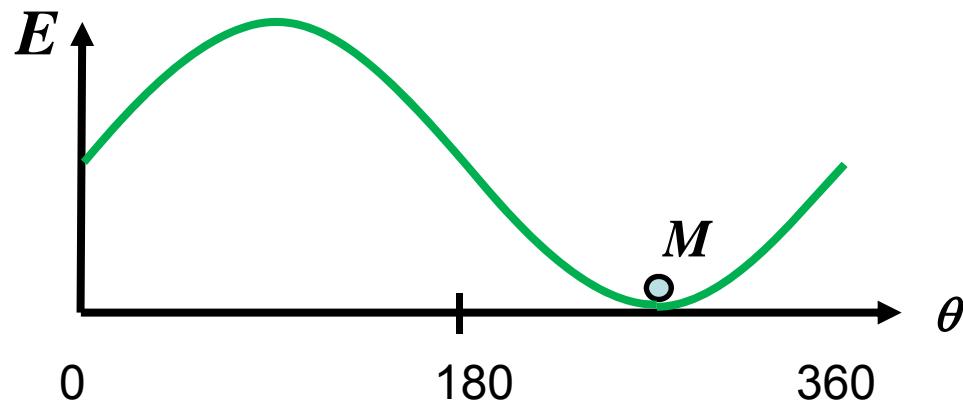
$$E_{anis} = K_u V \sin^2(\theta)$$

Magnetostatic energy

$$E_{ms} = H_{hard} M_s V \sin(\theta)$$



Total energy (Magnetic field along easy axis)



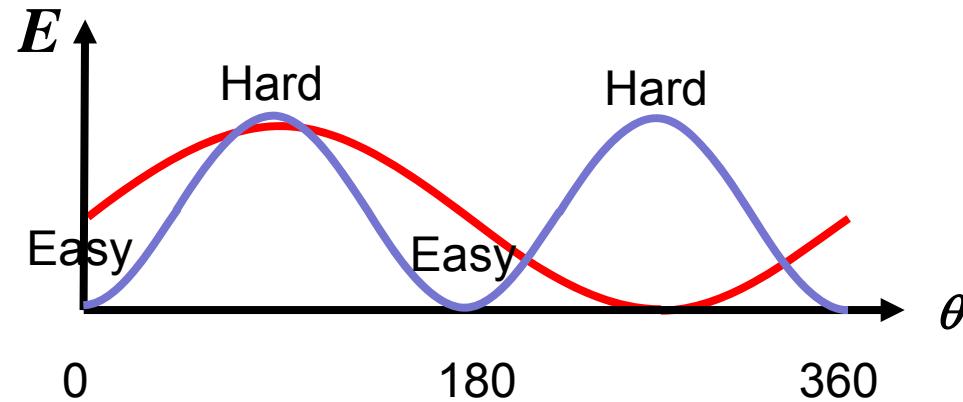
Stoner-Wohlfarth Theory*

Anisotropy energy

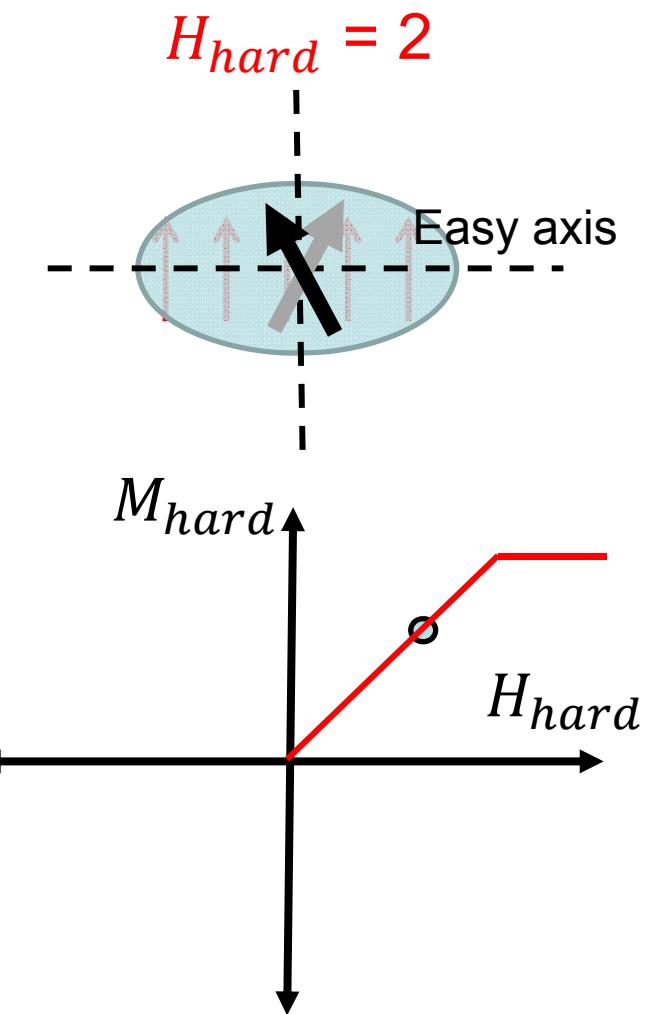
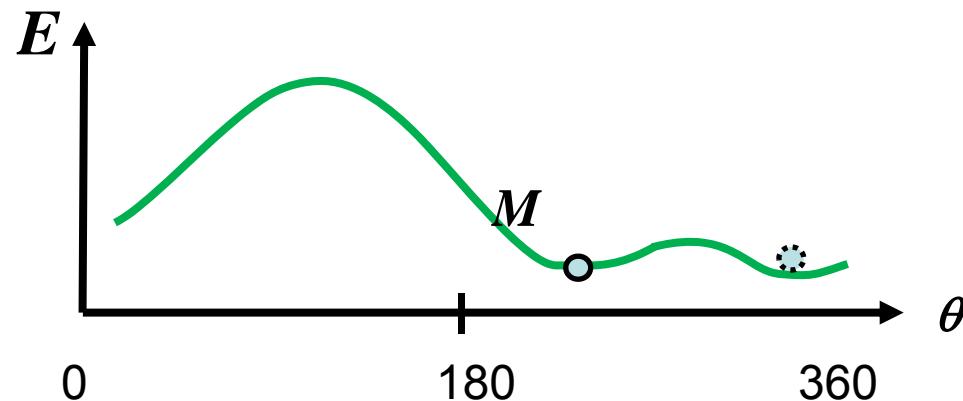
$$E_{anis} = K_u V \sin^2(\theta)$$

Magnetostatic energy

$$E_{ms} = H_{hard} M_s V \sin(\theta)$$



Total energy (Magnetic field along easy axis)



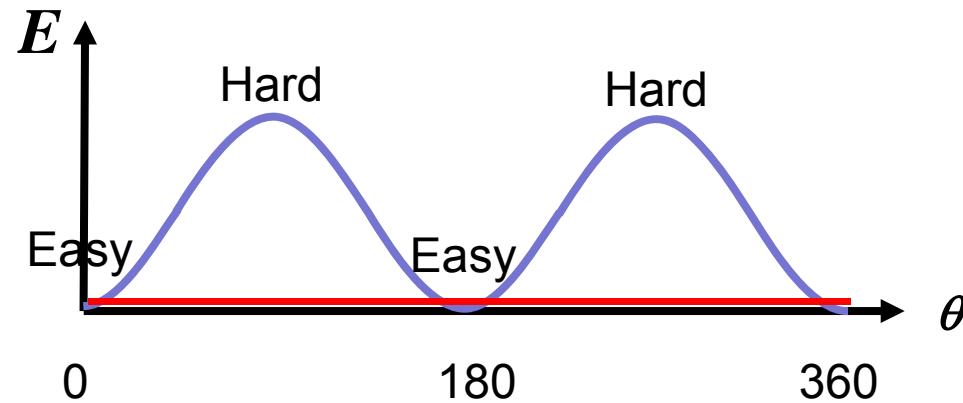
Stoner-Wohlfarth Theory*

Anisotropy energy

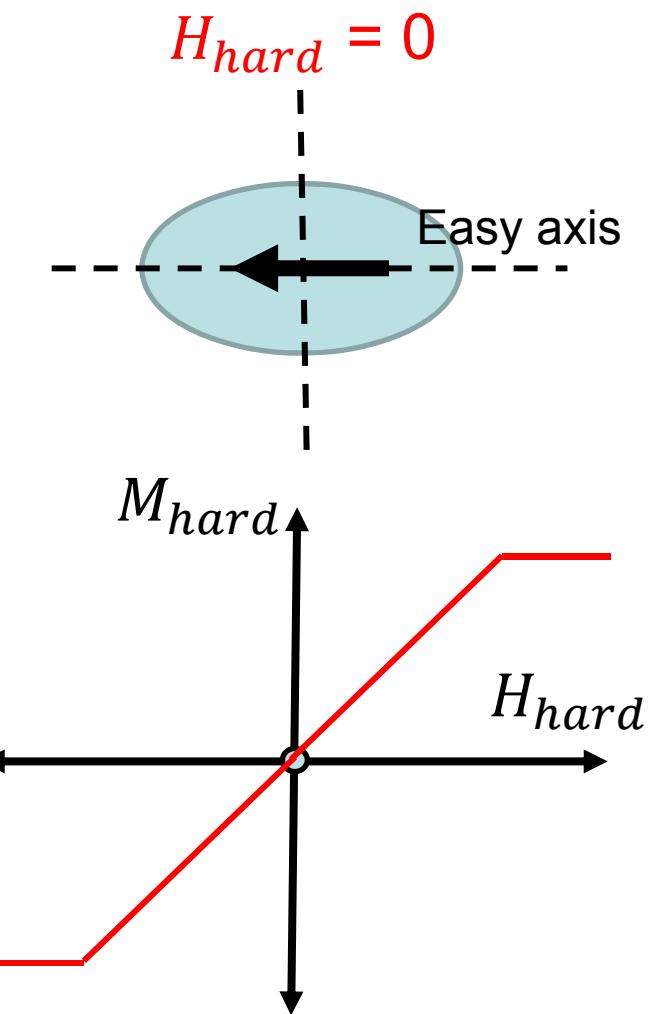
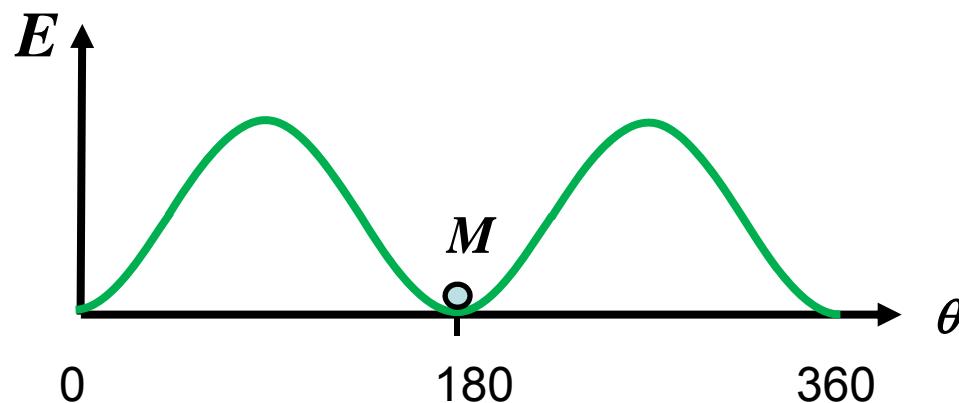
$$E_{anis} = K_u V \sin^2(\theta)$$

Magnetostatic energy

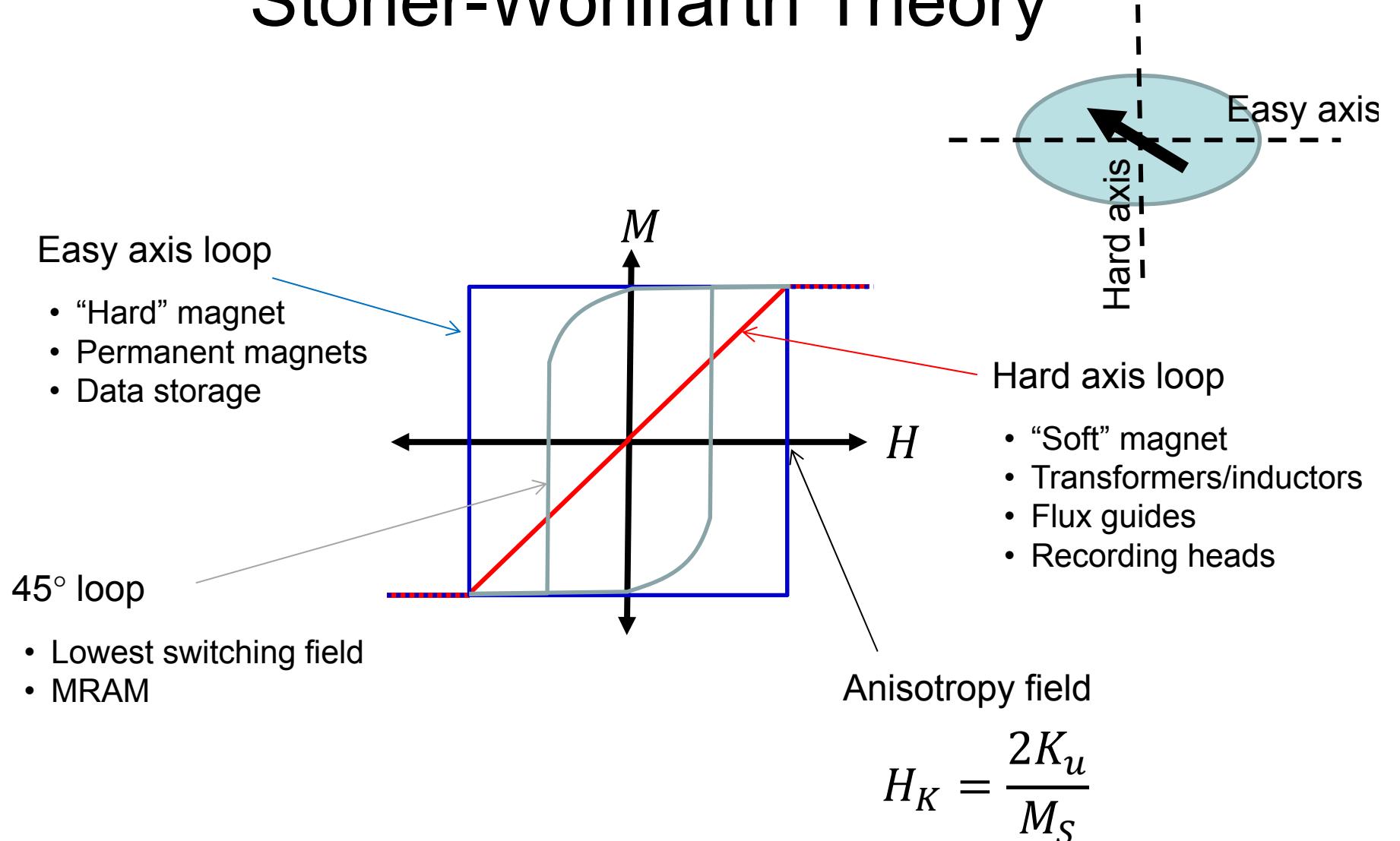
$$E_{ms} = H_{hard} M_s V \sin(\theta)$$



Total energy (Magnetic field along easy axis)



Stoner-Wohlfarth Theory

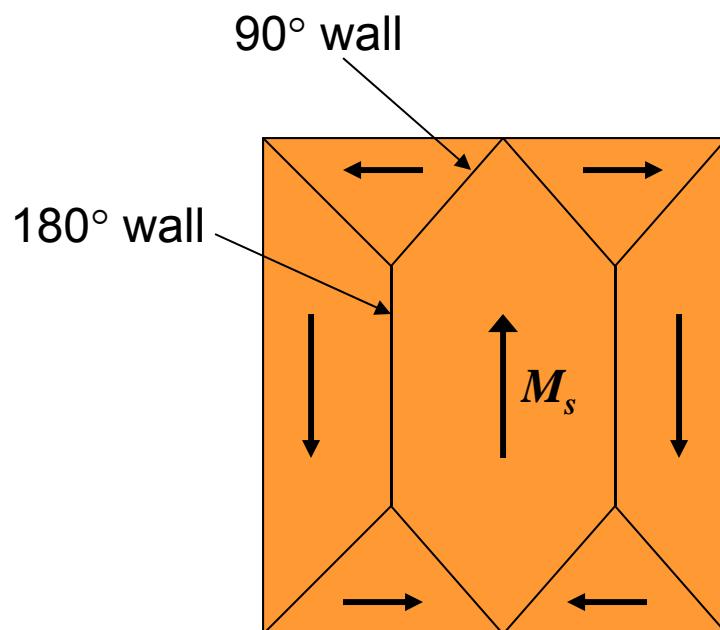


$$H_K = \frac{2K_u}{M_S}$$

Magnetic Domains

Domain Walls

Domain walls are the boundary between two regions with different magnetization direction.

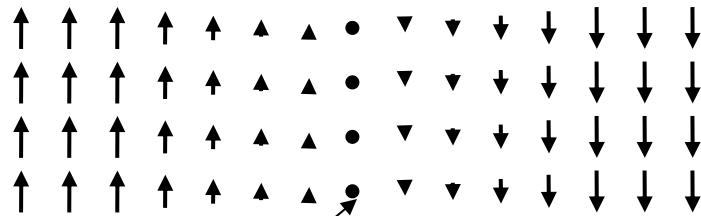


- A ferromagnet with net magnetization less than saturation breaks into domains due to demagnetizing fields.
- Domains form to reduce the magnetostatic energy.
- Within a domain, the magnitude of magnetization is the “spontaneous magnetization”, M_s
- The direction of magnetization varies from domain to domain.

Two Types of Domain Walls

- Bloch wall

magnetization rotates around axis normal to wall



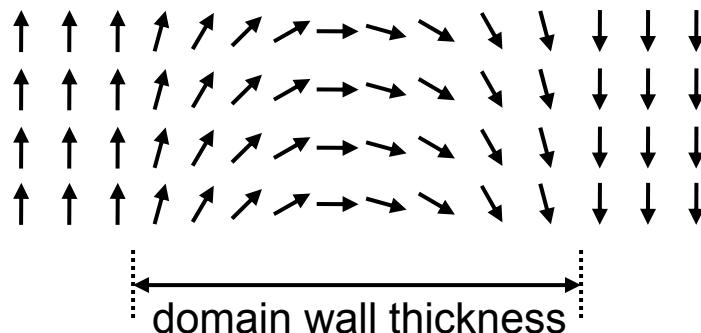
M pointing at you !

$$\text{div}(M) = 0 \Rightarrow \text{no poles in bulk}$$



Felix Bloch
(1905-1983)

- Néel wall



$$\text{div}(M) \neq 0 \Rightarrow \text{distributed poles in bulk}$$



Scanned at the American
Institute of Physics

Louis Néel
(1904-2000)

Domain Wall Exchange Energy

- Assume linear transition over N lattice points

$$\theta(n) = \pi \frac{n}{N} \quad \text{for } n = 0..N$$

- Angle between adjacent moments is

$$\Delta\theta = \frac{\pi}{N}$$

- Exchange energy between adjacent moments

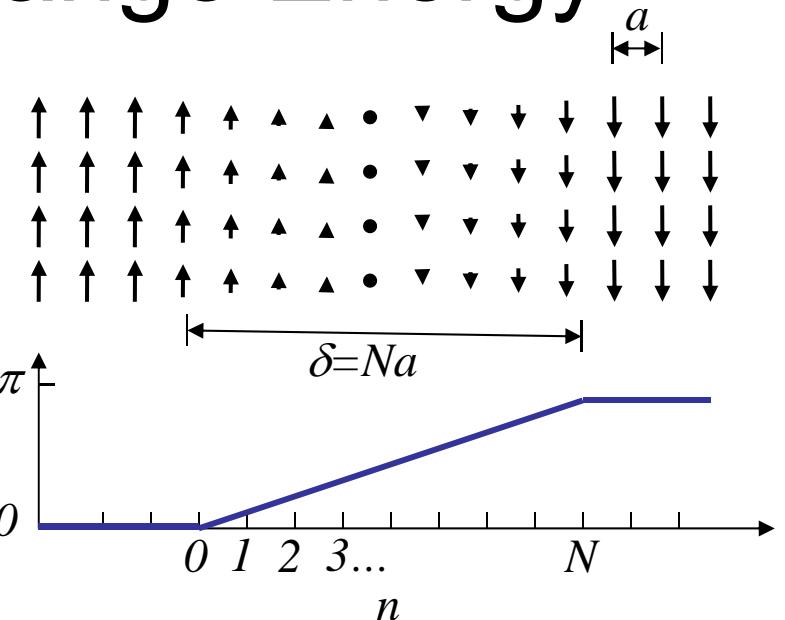
$$E_{m_i, m_{i+1}} = -\mu_0 \mathcal{J} m^2 \cos(\Delta\theta) \cong -\mu_0 \mathcal{J} m^2 \left(1 - \frac{(\Delta\theta)^2}{2}\right)$$

- Summing through wall thickness

$$\begin{aligned} \sum_{n=0..N} E_{m_n, m_{n+1}} &= \frac{N \mu_0 \mathcal{J} m^2 (\Delta\theta)^2}{2} + C \\ &= \frac{\mu_0 \mathcal{J} m^2 \pi^2}{2N} + C \end{aligned}$$

- Summing over wall area:

$$E_{exch} = \frac{\text{Area}}{a^2} \frac{\mu_0 \mathcal{J} m^2 \pi^2}{2N} + C$$



- Using $\delta = Na$:

$$\frac{E_{exch}}{\text{Area}} = \frac{\mu_0 \mathcal{J} m^2 \pi^2}{2a} \frac{1}{\delta}$$

- Exchange energy favors thick walls.

Domain Wall Anisotropy Energy

- Assume linear transition over N lattice points

$$\theta(n) = \pi \frac{n}{N} \quad \text{for } n = 0..N$$

- Anisotropy energy penalty for each moment:

$$E_{m_i} = K_u \sin^2(\theta) a^3$$

uniaxial anisotropy energy / volume

- Summing through wall thickness

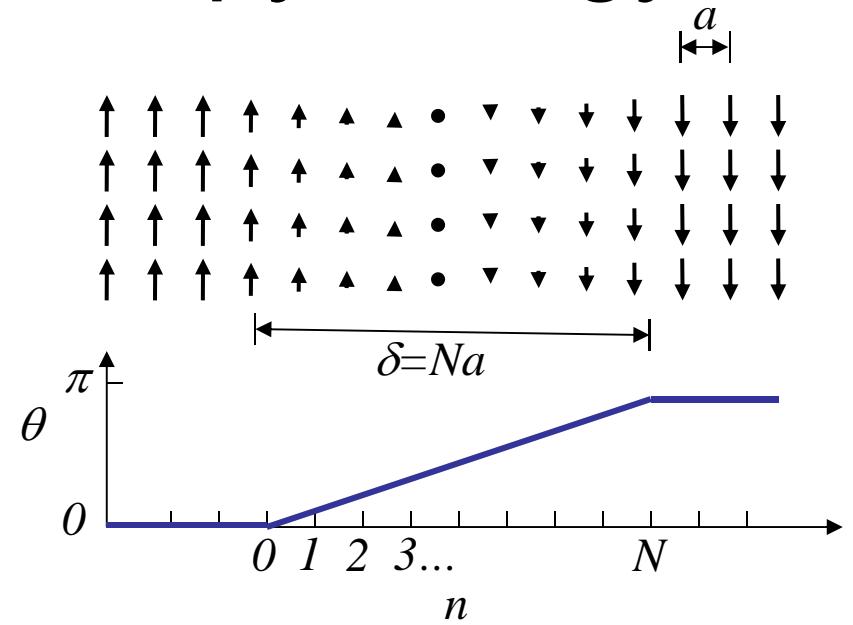
$$\sum_{n=0..N} E_{m_n} \cong \frac{N}{\pi} \int_0^\pi K_u \sin^2(\theta) a^3 d\theta = \frac{K_u N a^3}{2}$$

- Summing over wall area:

$$E_{anis} = -\frac{\text{Area}}{a^2} \frac{K_u N a^3}{2}$$

Or,

$$\frac{E_{anis}}{\text{Area}} = \frac{K_u}{2} \delta$$



- Anisotropy energy favors thin walls.

Domain Wall Thickness

- Domain wall thickness is determined by a balance between anisotropy and exchange energy:

$$\frac{E_{anis}}{\text{Area}} = \frac{K_u}{2} \delta \quad \frac{E_{exch}}{\text{Area}} = \frac{\mu_0 \mathcal{J} m^2 \pi^2}{2a} \frac{1}{\delta}$$

- Define exchange stiffness: $A = \frac{\mu_0 \mathcal{J} m^2}{a}$
- Total wall energy is:

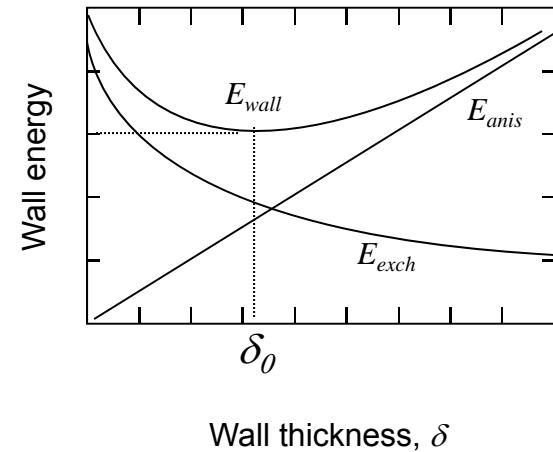
$$\frac{E_{wall}}{\text{Area}} = \frac{K_u}{2} \delta + \frac{\pi^2 A}{2\delta}$$

- The minimum energy is achieved at:

$$\frac{dE_{wall}}{d\delta} = \frac{K_u}{2} - \frac{\pi^2 A}{2\delta^2} = 0 \Rightarrow \delta_0 = \pi \sqrt{\frac{A}{K_u}}$$

- Where the wall energy is:

$$E_{wall} = \pi \sqrt{K_u A} \text{ Area}$$

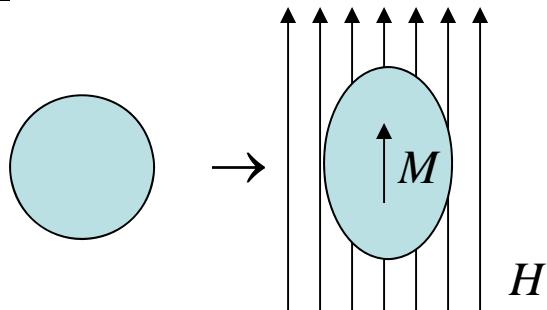


Magnetostriction

Random crystal orientation:

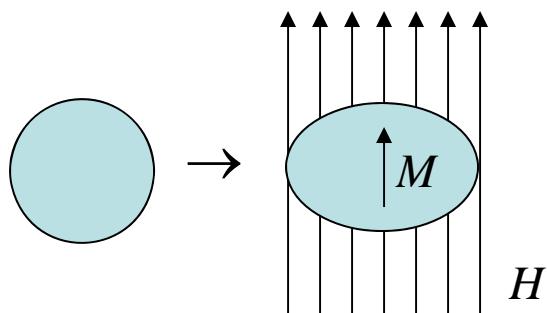
$$\frac{\Delta l}{l} = \frac{3}{2} \lambda_s (\cos^2 \theta - \frac{1}{3})$$

$$\underline{\lambda_s > 0}$$



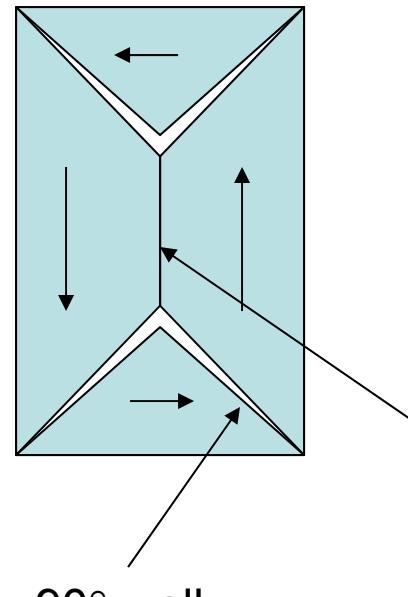
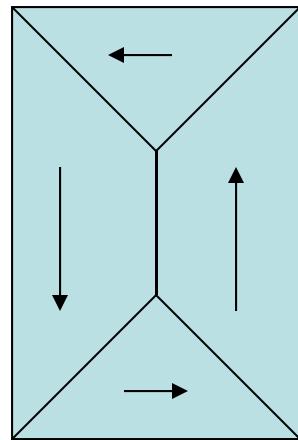
E.g. “Terfenol”
 TbFe_2 : $\lambda_s = 1753 \times 10^{-6}$

$$\underline{\lambda_s < 0}$$



E.g.
Ni (fcc): $\lambda_s = -34 \times 10^{-6}$
Fe (bcc): $\lambda_s = -7 \times 10^{-6}$

Magnetostrictive Effect on Domain Walls



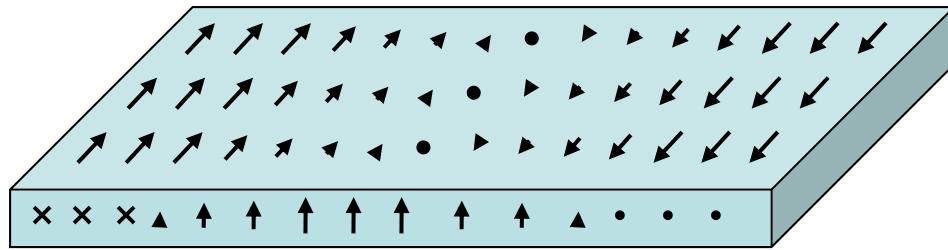
180° wall

90° wall

- Magnetostrictive strain energy favors 180 degree walls.

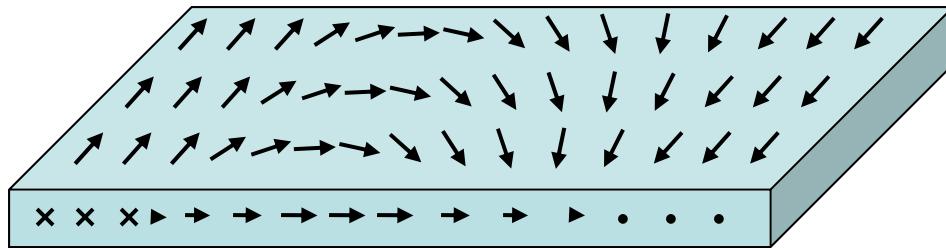
Domain Walls in Thin Films

- Bloch wall

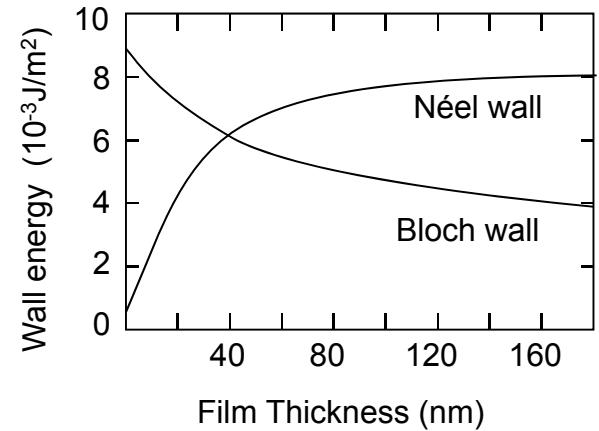


Magnetic poles on surface

- Néel wall



Magnetic poles in bulk

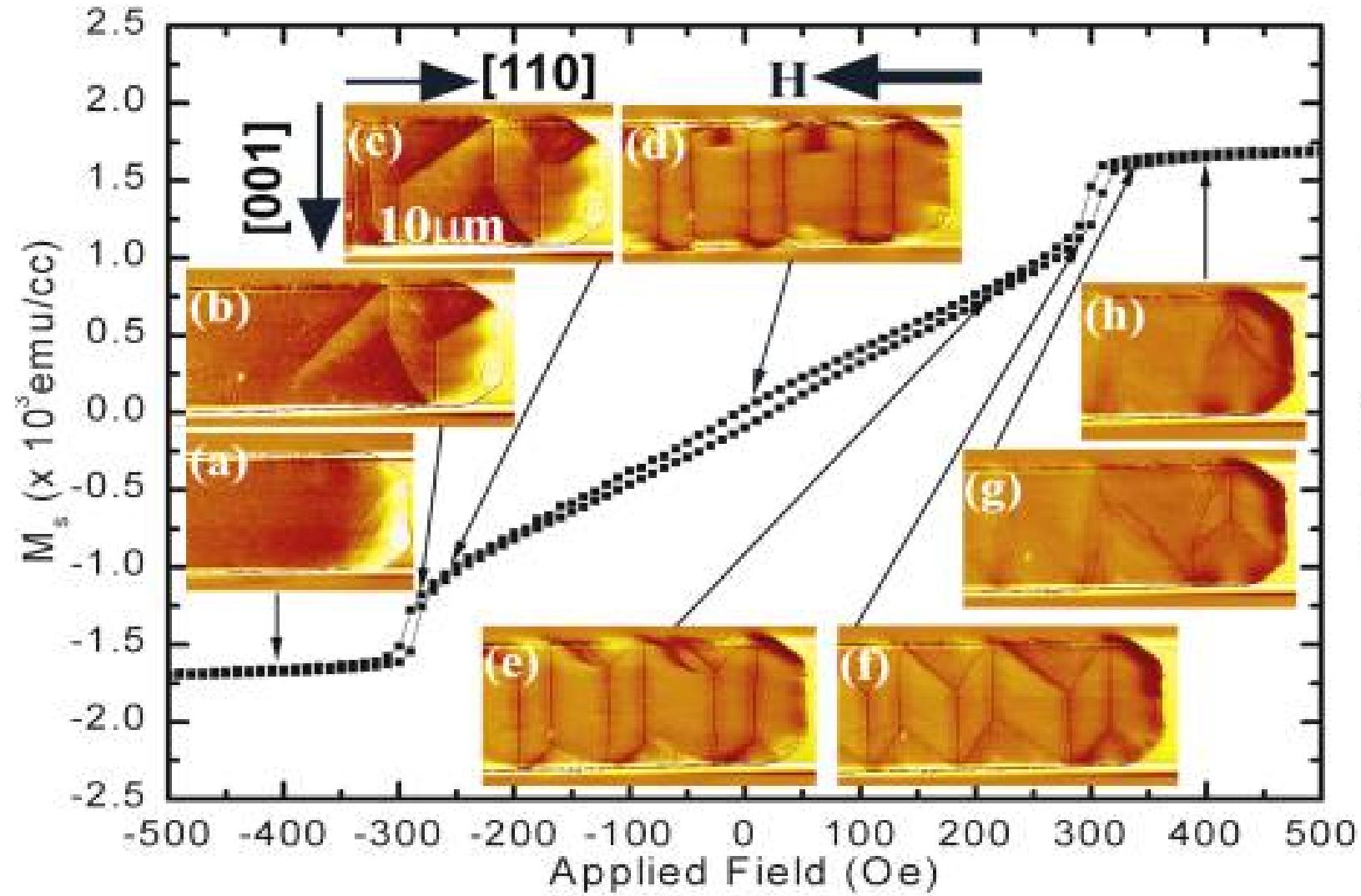


For $A = 10^{-11} \text{ J/m}$, $B_s = 1 \text{ T}$ and $K = 100 \text{ J/m}^3$
from O'Handley, Modern Magnetic Materials

Domain Configuration

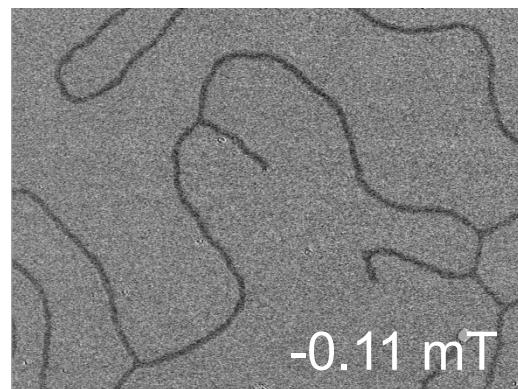
- Balance of energy between:
 - Magnetostatic self energy (demag. field -> try to reduce magnetic poles)
 - Domain wall energy (exchange and anisotropy -> reduce wall area)
 - Strain energy (magnetostriiction -> favor 180° walls)
 - Magnetostatic energy in applied field ($E = -m \cdot B$ -> favors alignment with field)

Domains in Fe film

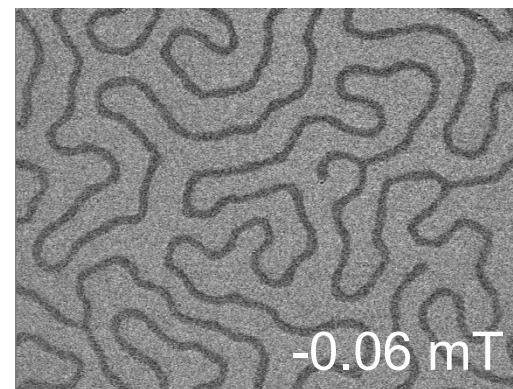


MFM images From: <http://physics.unl.edu/~shliou/ResearchActivity/research3.htm>

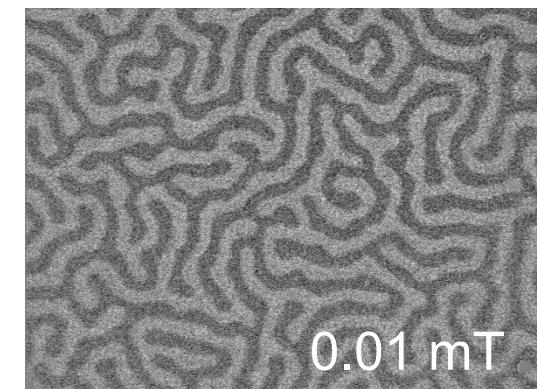
Stripe domains in CoFeB thin film with Perpendicular Anisotropy



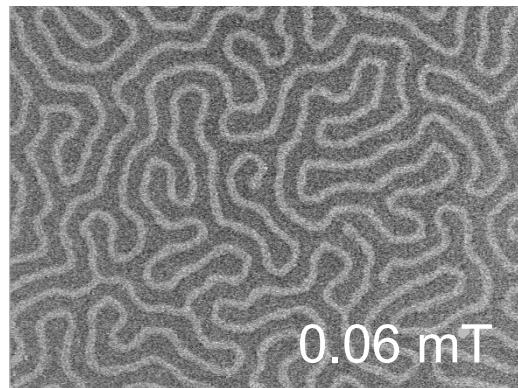
-0.11 mT



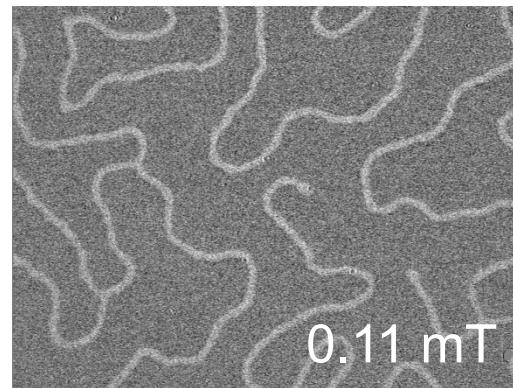
-0.06 mT



0.01 mT



0.06 mT



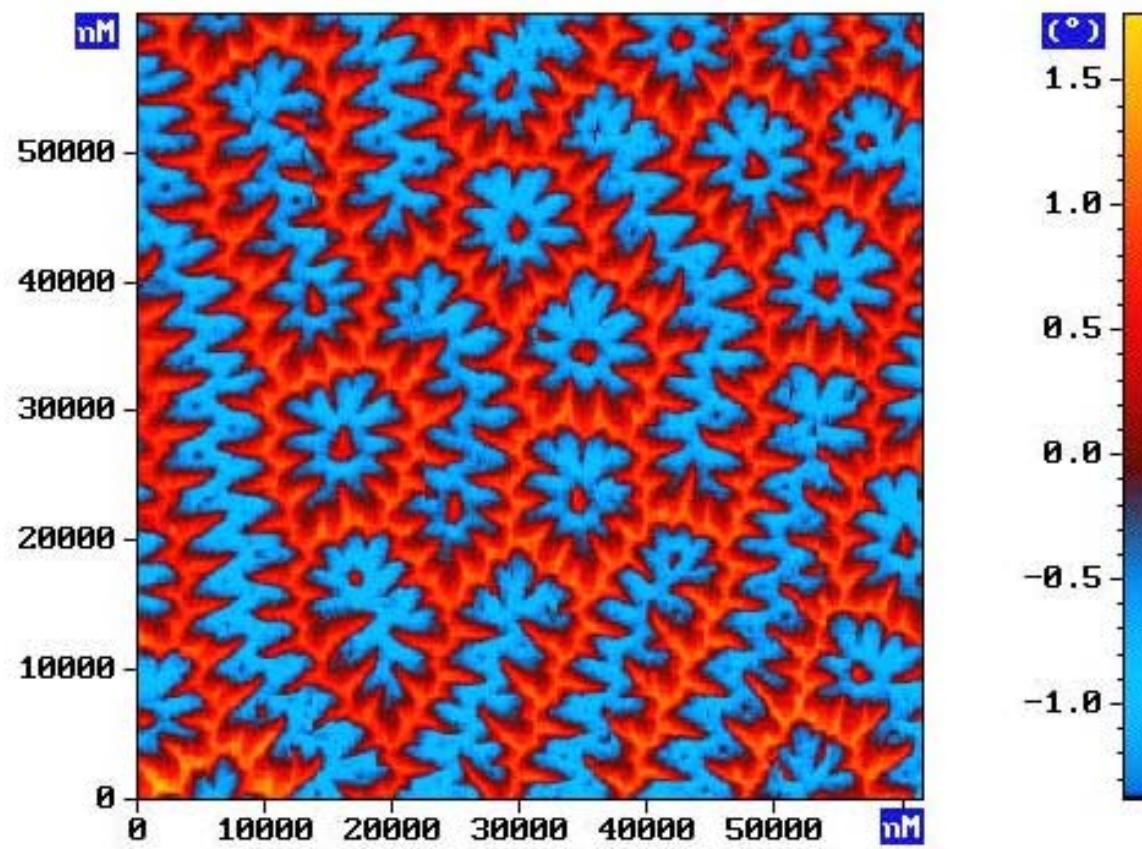
0.11 mT

—
25 μm

Polar Kerr images.

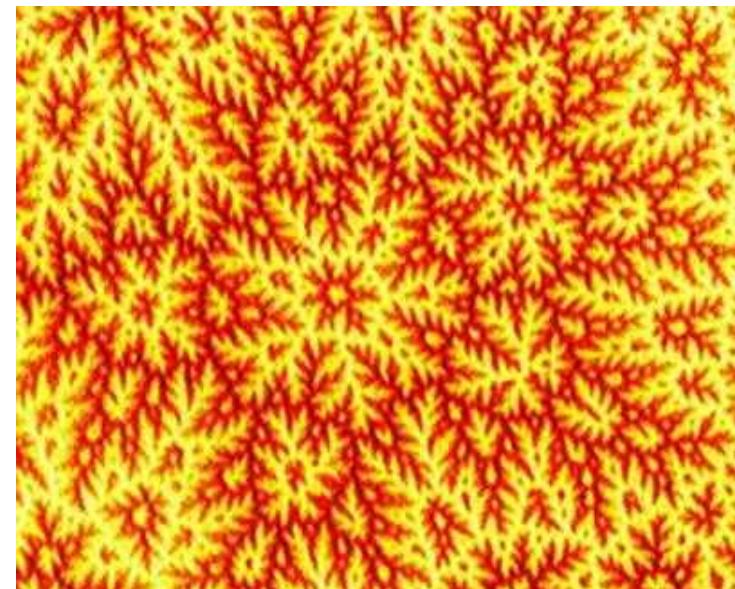
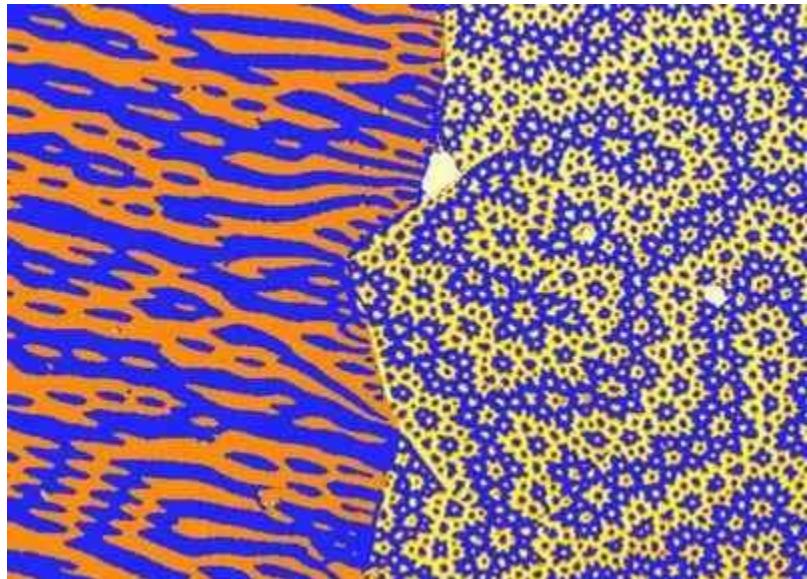
Flower Domains in YIG

MFM Image



From: http://www.nanoworld.org/russian/s_11.html

Pretty Domain Patterns

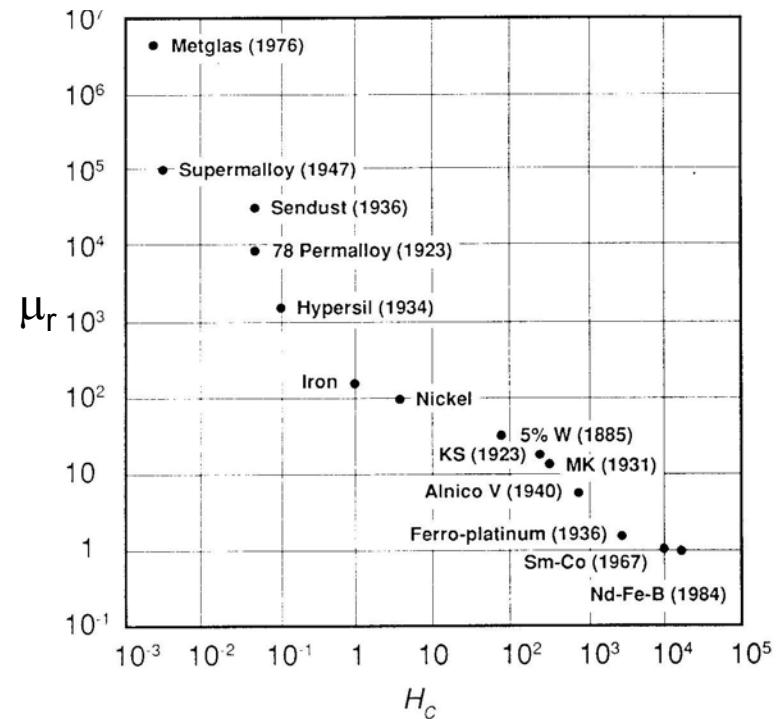
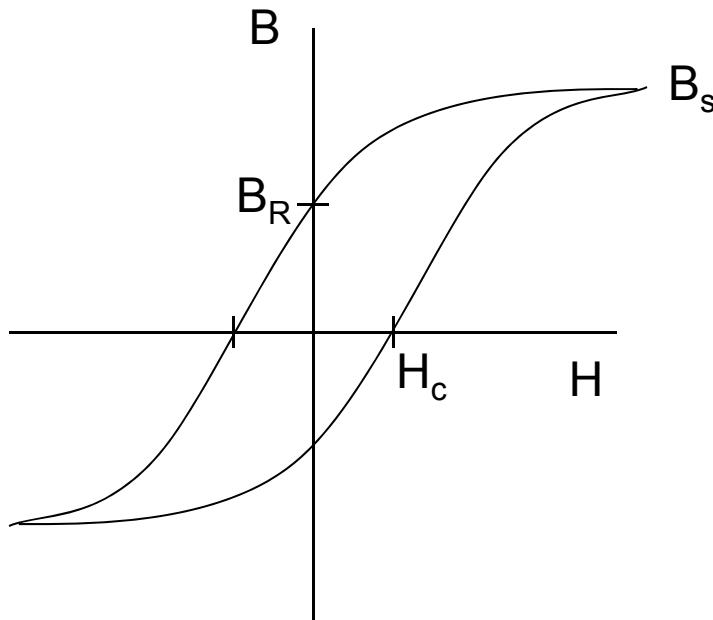


Magnetic Materials

Magnetic materials are typically classified as “hard” or “soft” depending on the intended application.

Soft magnets have low coercivity and high permeability.

Hard magnets have high coercivity and high remanent magnetization.



Soft Iron

- Inexpensive, high coercivity material
- $\mu_r \sim 1000 - 5000$
- Used in DC/low frequency applications

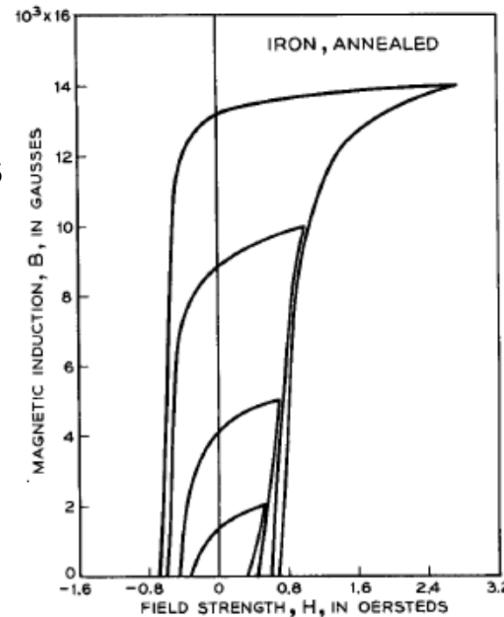
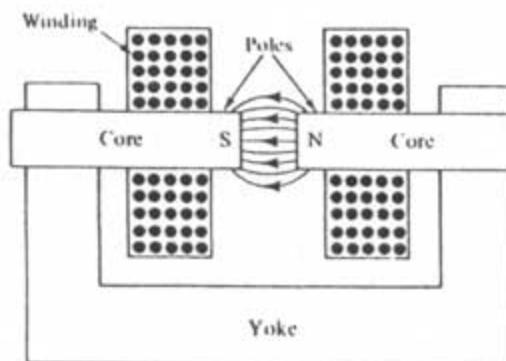


FIG. 3-5. Upper halves of hysteresis loops of ordinary annealed iron



Silicon Steel (“Electrical Steel”)

- Most common in power (50/60 Hz) applications
- Adding Si, Al increases resistivity, permeability and reduces coercivity.
- Bad effects: reduces B_s , T_c and increases brittleness
- Higher resistivity and lower coercivity -> less losses
- Higher permeability -> better coupling
- Si limited to 3-4%, material gets too brittle.

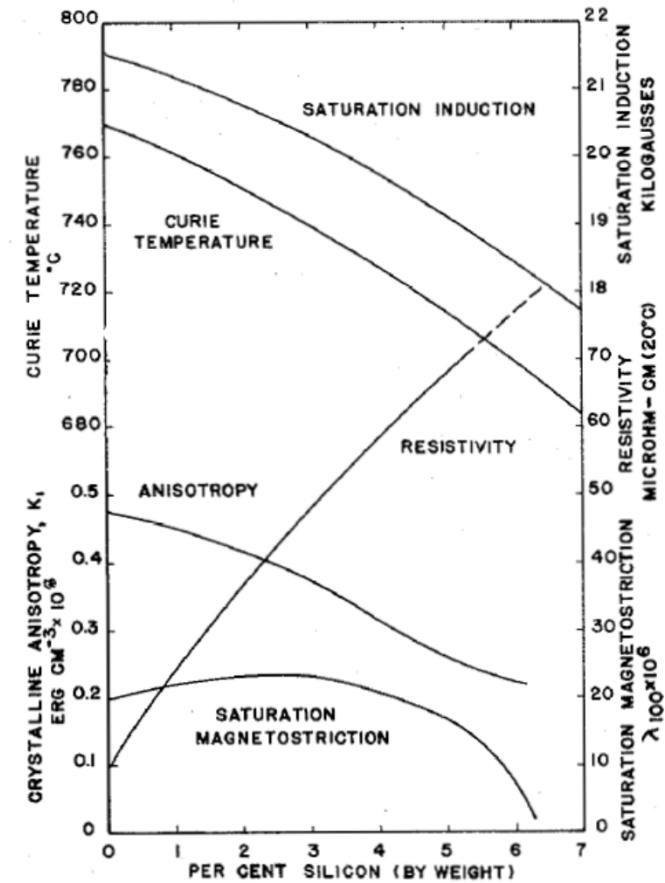
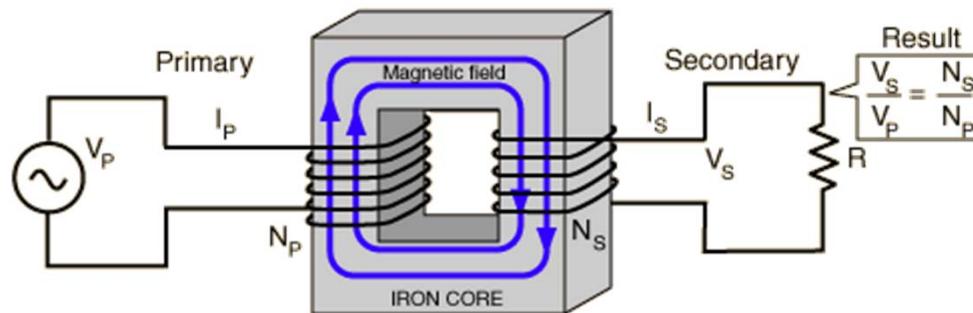


Fig. 1. Variation of important properties of silicon-iron alloys with composition.

Littmann, M.; Iron and silicon-iron alloys,
IEEE Transactions on Magnetics, 7, 48 - 60 (1971)

Cold-rolled Grain-Oriented Steel (CRGO)

- Reduces hysteresis further by orienting grains:

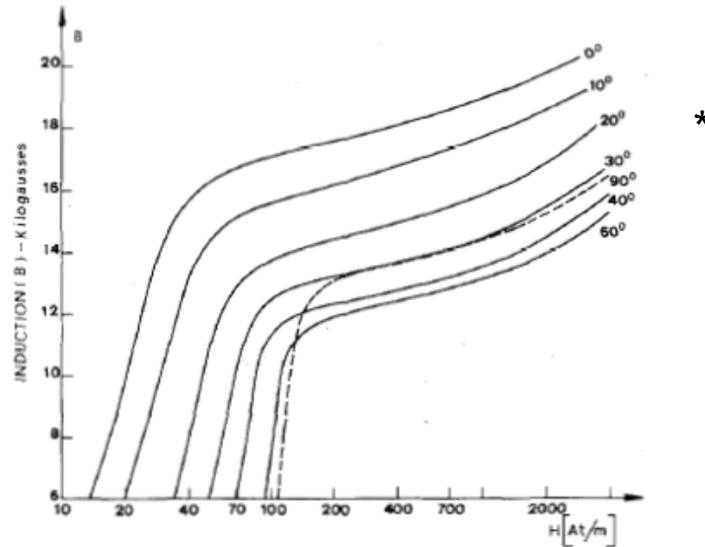


Fig. 2. AC excitation curve, induction at various angles to rolling direction.

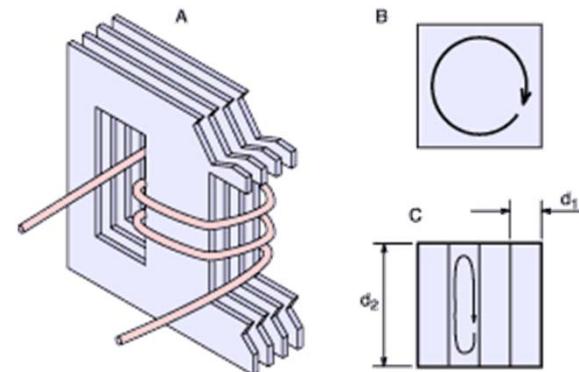
Commercial iron
Si-Fe hot rolled
Si-Fe CRGO

| | <u>Losses (W/kg)</u> |
|------------------|----------------------|
| Commercial iron | 5-10 |
| Si-Fe hot rolled | 1-3 |
| Si-Fe CRGO | 0.3-0.6 |

*Di Napoli, A.; Paggi, R.; A model of anisotropic grain-oriented steel, IEEE Transactions on Magnetics 19, 1557, (1983)



Lamination reduces eddy currents:



Ni-Fe Alloys (Permalloys)

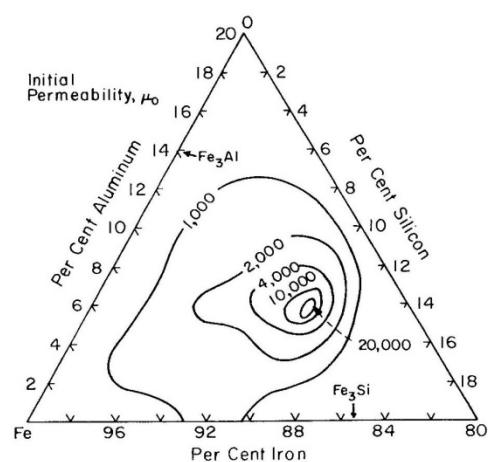
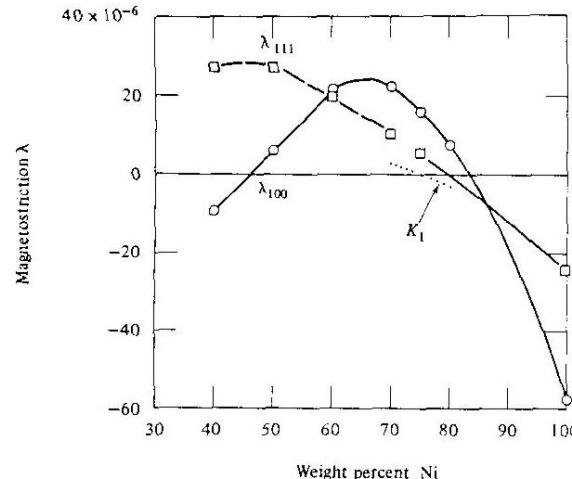


Figure 10.11 Contours of initial permeability on same Fe-Si-Al ternary diagram as Figure 10.10 (Bozorth, IEEE Press, copyright 1994).



2.12 Dependence of magnetostriction coefficients λ_{100} and λ_{111} with nickel content for nickel alloys.

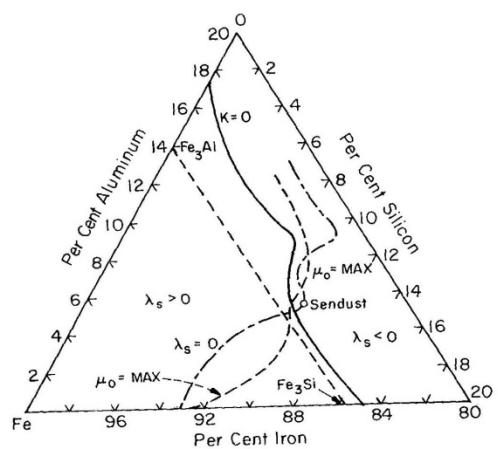


Figure 10.10 Iron-rich corner of ternary Fe-Si-Al diagram (wt%) showing fields of positive and negative magnetostriction, the courses of the zero-anisotropy line and maximum permeability line. The Sendust composition is defined by the intersection of the $\lambda_s = 0$ and $K = 0$ lines (Bozorth, IEEE Press, copyright 1994).

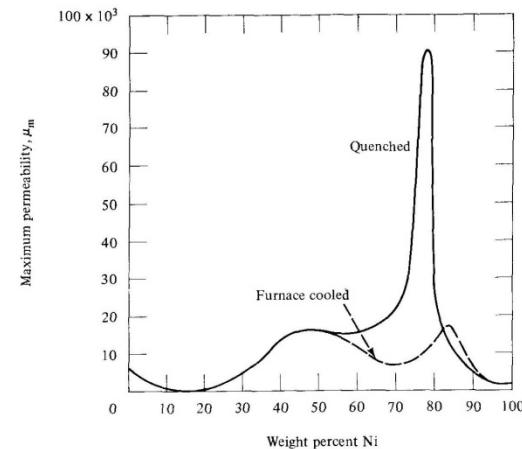


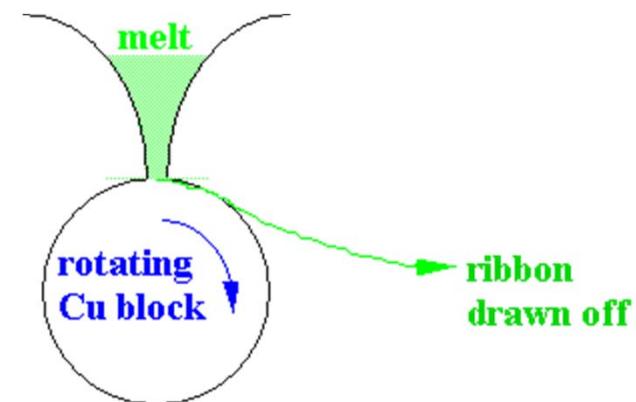
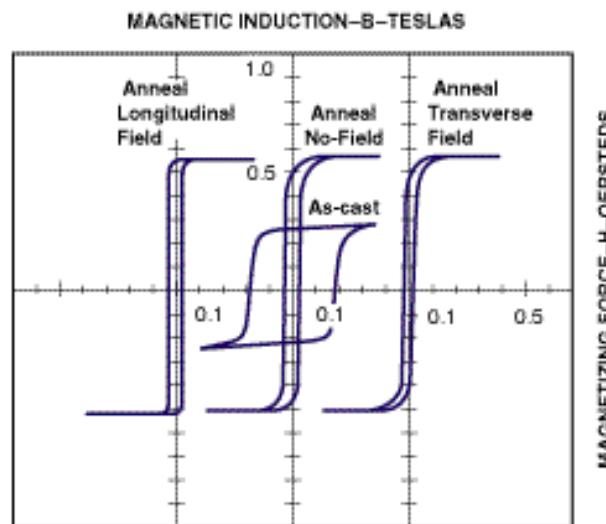
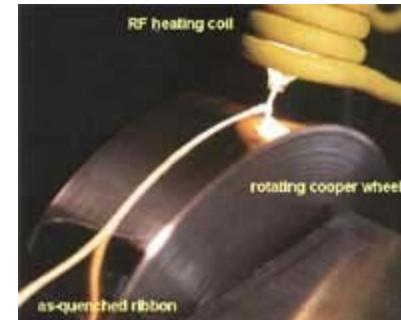
Fig. 13.26 Maximum permeabilities of iron-nickel alloys. Bozorth [13.30].

Zero magnetostriction
at 80%

Zero anisotropy
at 78%

Amorphous Alloys, “Metglas” (Metallic Glasses)

- No crystalline anisotropy
- Rapid quenching: melt spinning
- Ultra-low coercivity and super-high permeability
- Available in thin ribbons only:



Some Soft Magnetic Materials

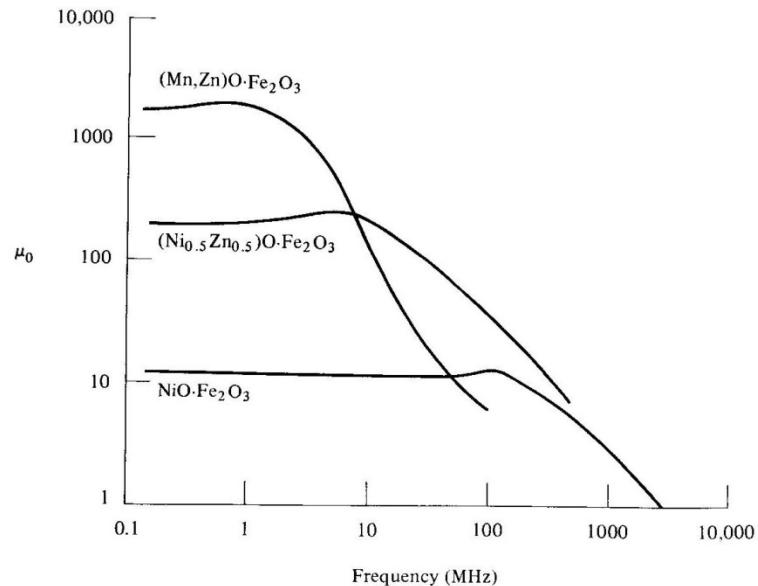
| Material | Composition | Relative Permeability | | H_c (kA/m) | B_s (T) |
|----------------------------------|--|-----------------------|-------------|-----------------|--------------|
| | | μ_i | μ_{max} | | |
| Iron | 100% Fe | 150 | 5000 | 80 | 2.15 |
| Silicon-iron (non-oriented) | 96% Fe 4% Si | 500 | 7000 | 40 | 1.97 |
| Silicon-iron (grain oriented) | 97% Fe 3% Si | 1500 | 40,000 | 8 | 2.0 |
| 78 Permalloy | 78% Ni 22% Fe | 8000 | 100,000 | 4 | 1.08 |
| Hipernik | 50% Ni 50% Fe | 4000 | 70,000 | 4 | 1.60 |
| Supermalloy | 79% Ni, 16% Fe 5% Mo | 100,000 | 1,000,000 | 0.16 | 0.79 |
| Mumetal | 77% Ni, 16% Fe 5% Cu, 2% Cr | 20,000 | 100,000 | 4 | 0.65 |
| Permendur | 50% Fe 50% Co | 800 | 5000 | 160 | 2.45 |
| Hiperco | 64% Fe, 35%Co 0.5% Cr | 650 | 10,000 | 80 | 2.42 |
| Supermendur | 49% Fe, 49%Co 2% V | - | 60,000 | 16 | 2.40 |
| Metglass (amorphous) | 1.6%Ni,4.4%Fe, 8.6%Si,82%Co, 3%B | - | 1,000,000 | 0.01 | 0.57 |

Ferrites

Ceramic materials of type $\text{MO}\cdot\text{Fe}_2\text{O}_3$ where M = transition metal

Magnetic properties are not as good as metals.

But, high resistivity makes them useful for high frequency applications.



Skin depth:

$$\delta = \frac{1}{\sqrt{\mu\sigma\pi f}}$$

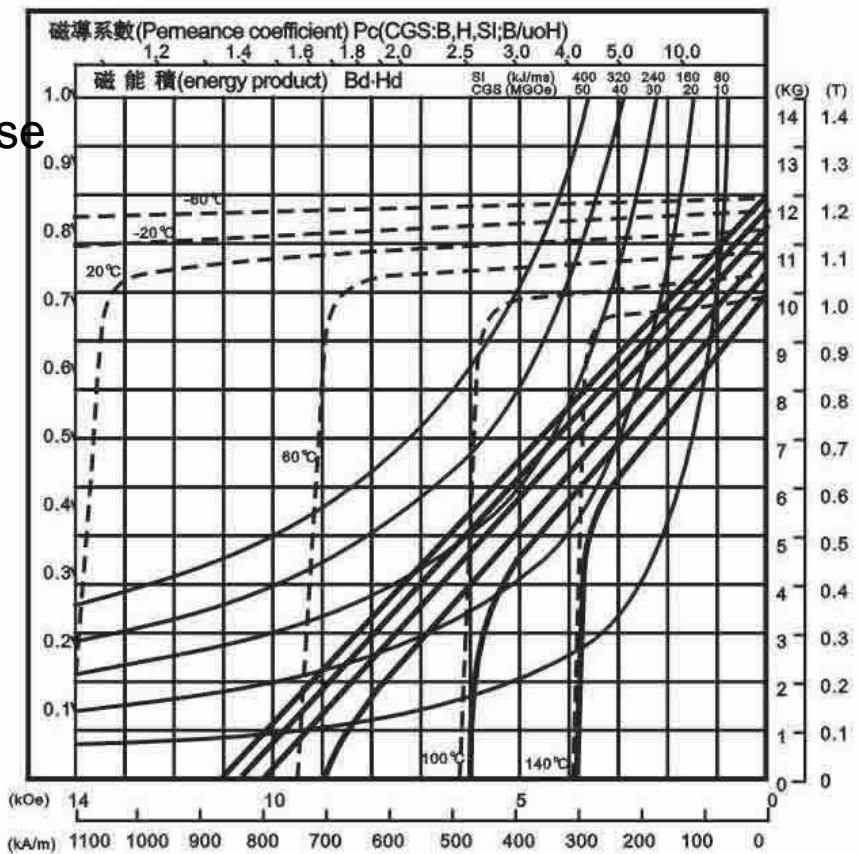
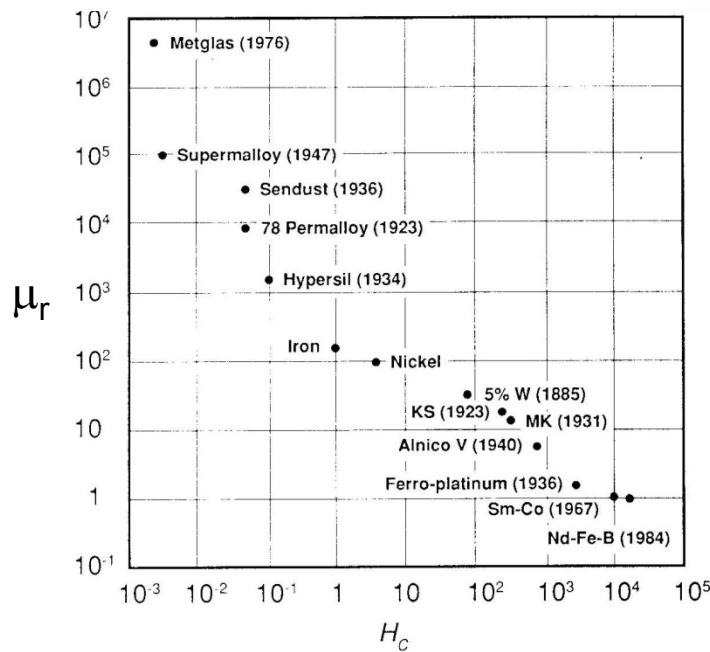
= 8.6 mm for Cu at 60 Hz

= 3 mm for Si-Fe at 60 Hz.

Fig. 13.42 Variation of initial permeability μ_0 with frequency for three ferrites.

Hard Magnetic Materials

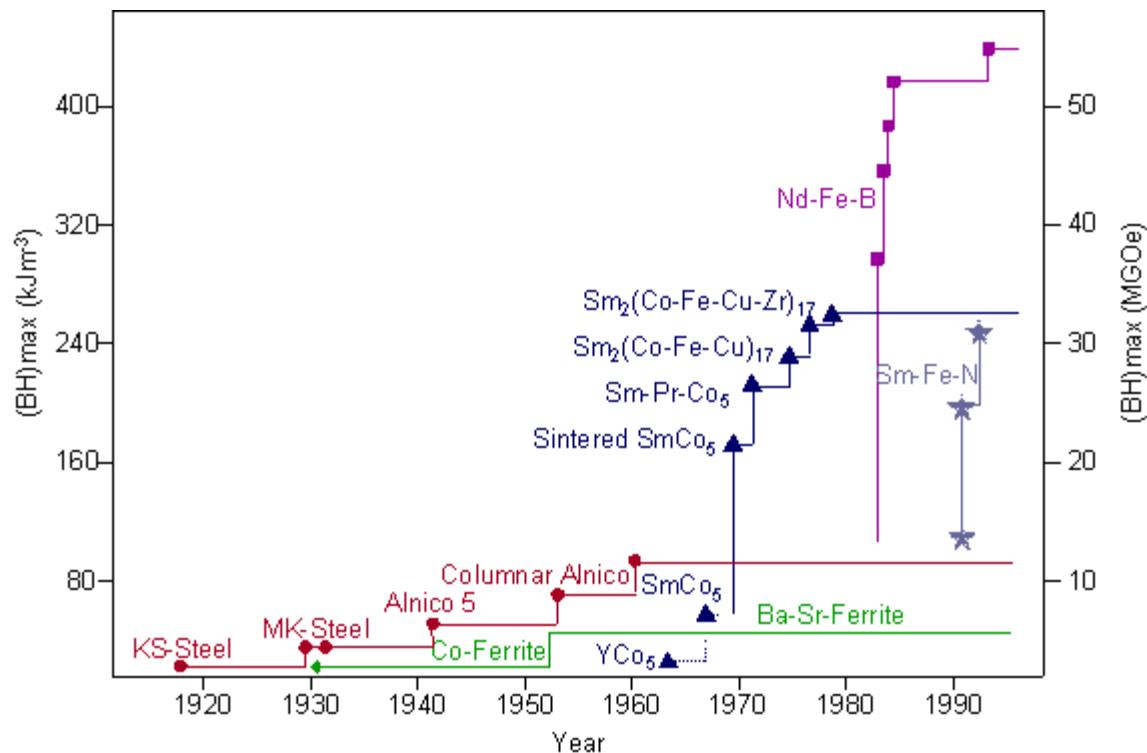
- Permanent magnet materials.
- Manufacturers typically provide data in the form of second quadrant B-H response or “demagnetisation curves”
- Often B and $\mu_0 M$ are plotted on same axis and often in CGS units.
- These days often in Chinese.



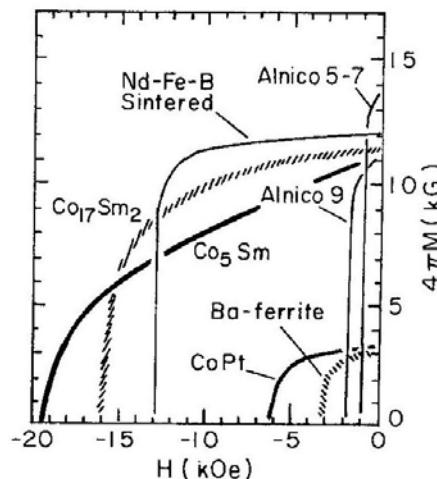
N-30

Demagnetization curves
of sintered magnet N30
at different temperatures

Advances in Permanent Magnet Materials



Common Permanent Magnet Materials

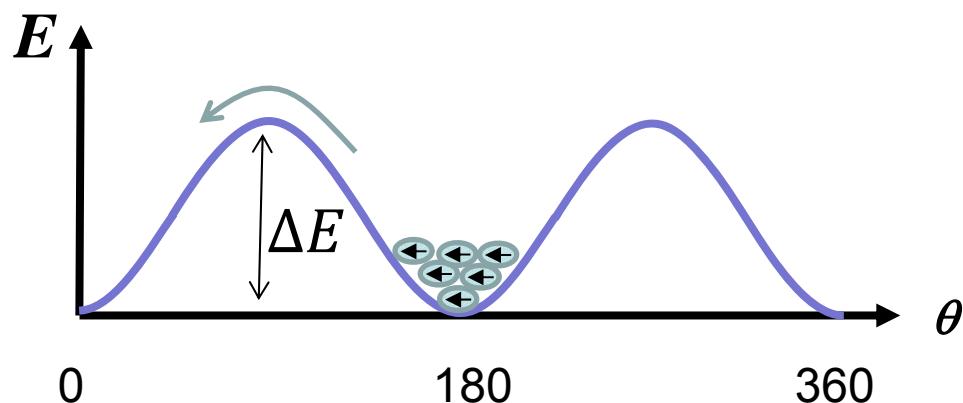


| Material | B_r (T) | H_c (kA/m) | $(BH)_{max}$ (kJ/m ³) | T_c of B_r (%/°C) | T_{max} (°C) | T_{curie} (°C) | Cost (relative) | Notes |
|----------|-----------|--------------|-----------------------------------|-----------------------|----------------|------------------|-----------------|------------------|
| SmCo | 1.05 | 730 | 206 | -0.04 | 300 | 750 | Highest (100) | Hard, brittle |
| NdFeB | 1.28 | 980 | 320 | -0.12 | 150 | 310 | High (50) | Corrodes easily |
| Alnico | 1.25 | 50 | 45 | -0.02 | 540 | 860 | Medium (30) | |
| Ferrite | 0.39 | 250 | 28 | -0.20 | 300 | 460 | Low (5) | |
| Bonded | 0.25 | 160 | 11 | -0.19 | 100 | - | Low (1) | Injection molded |

Thermal Decay of Magnetization

Superparamagnetism

For $H_a=0$:



$$\Delta E = K_u V$$

$$M(t) = M_0 e^{-t/\tau}$$

$$\tau = \tau_0 e^{-\Delta E / k_B T}$$

τ_0 = attempt period $\sim 1\text{ns}$

“Superparamagnetic” if $K_u V < k_B T$